

Multiscale Discretizations for Flow, Transport, and Mechanics in Porous Media

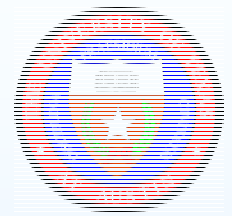
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Acknowledge
Todd Arbogast, Vivette Girault, Shuyu Sun, Tim Wildey, and Ivan Yotov,



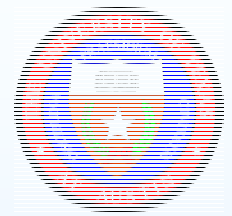
Outline



- ◆ Motivation
- ◆ Mortar mixed finite element (MMFE) methods for multiphase flow problem
- ◆ Time splitting for MMFE for multiphase flow and mixed/Godunov methods for diffusion-dispersion and reactive transport
- ◆ Numerical experiments
- ◆ Extensions to DG and DG-MMFE for flow and Galerkin for elasticity
- ◆ Conclusions
- ◆ Current and Future Work



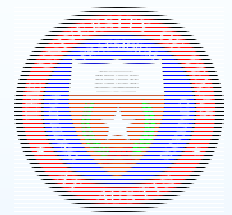
Motivation



- ◆ Goal is to solve heterogeneous subsurface flow problems: multiphase flow, coupled with reactive transport and geomechanics in a multiscale setting.
- ◆ Applications: NAPL remediation, monitoring of nuclear wastes, CO₂ sequestration saline aquifers.
- ◆ Traditional method - uniform grid everywhere, too expensive. Mortars lead to attractive dynamic meshing strategies and multiphysics couplings.
- ◆ Cannot avoid if physical domain is irregular! No single smooth map to a regular computational grid exists.



Societal Needs in Relation to Geological Systems



Resources Recovery

- Petroleum and natural gas recovery from conventional/unconventional reservoirs
- *In situ* mining
- Hot dry rock/enhanced geothermal systems
- Potable water supply
- Mining hydrology

Waste Containment/Disposal

- Deep waste injection
- Nuclear waste disposal
- CO₂ sequestration
- Cryogenic storage/petroleum/gas

Underground Construction

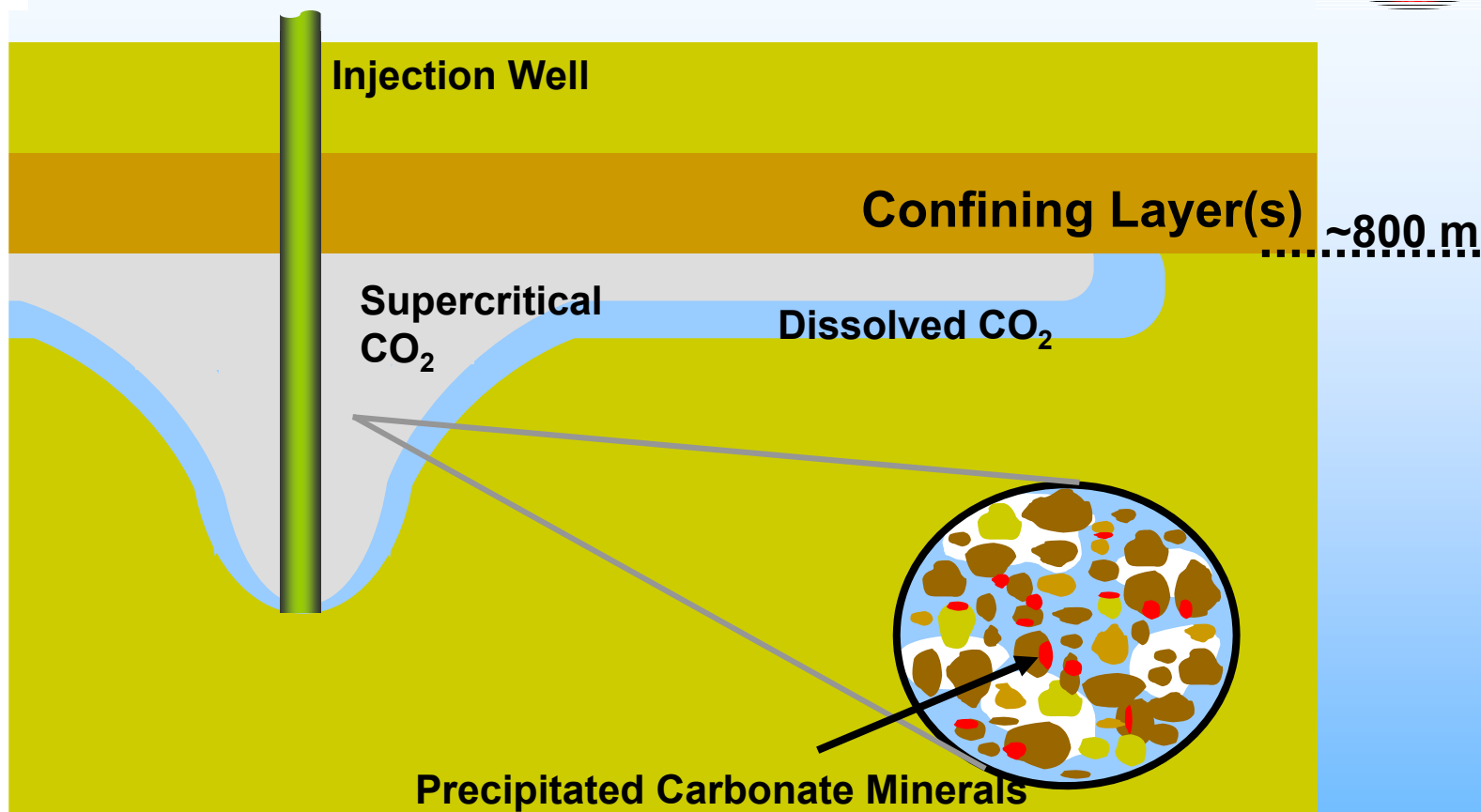
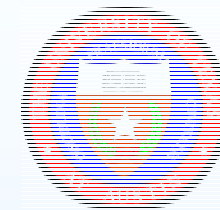
- Civil infrastructure
- Underground space
- Secure structures

Site Restoration

- Aquifer remediation
- Acid-rock drainage



CO₂ Injection and Trapping Mechanisms



**Stratigraphic
Trapping**

**Solubility
Trapping**

**Hydrodynamic
Trapping**

**Mineral
Trapping**

$$\frac{\partial(\varphi_i^* c_{iw})}{\partial t} - \nabla \cdot \mathbf{D}_i^* \nabla c_{iw} = 0$$

Solved fully-implicitly using **Expanded MFEM** with full-tensor

Introduce $\tilde{\mathbf{z}} = -\nabla c$, $\mathbf{z} = \mathbf{D}_i^* \tilde{\mathbf{z}}$

Find $\tilde{\mathbf{z}}_{h,iw}^{m+1}|_{\Omega_j} \in \tilde{\mathbf{V}}_{h,j}$, $\mathbf{z}_{h,iw}^{m+1}|_{\Omega_j} \in \mathbf{V}_{h,j}$, $c_{h,iw}^{m+1}|_{\Omega_j} \in W_{h,j}$ such that:

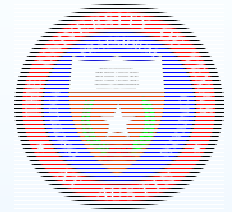
$$\left(\frac{\varphi_i^{*,m+1} c_{h,iw}^{m+1} - \hat{T}_i}{\Delta \tau^{m+1}}, w \right)_{\Omega_j} + (\nabla \cdot \mathbf{z}_{h,iw}^{m+1}, w)_{\Omega_j} = 0, w \in W_{h,j}$$

$$(\tilde{\mathbf{z}}_{h,iw}^{m+1}, \mathbf{v})_{\Omega_j} = (c_{h,iw}^{m+1}, \nabla \cdot \mathbf{v})_{\Omega_j} - \langle \mathcal{P}_j c_{h,iw}, \mathbf{v} \cdot \mathbf{n}_j \rangle_{\Gamma_j}, \mathbf{v} \in \mathbf{V}_{h,j}$$

$$(\mathbf{z}_{h,iw}^{m+1}, \tilde{\mathbf{v}})_{\Omega_j} = (\mathbf{D}_i^{*,m+1} \tilde{\mathbf{z}}_{h,iw}^{m+1}, \tilde{\mathbf{v}})_{\Omega_j}, \tilde{\mathbf{v}} \in \tilde{\mathbf{V}}_{h,i}$$



Simplifying Assumptions



- ◆ Flow is independent of transport.
- ◆ Inter-phase distribution of species assumed to be ``locally equilibrium" controlled, instantaneously.
- ◆ Ignore adsorption.

$\bar{\Omega} = \cup_{i=1}^{n_b} \bar{\Omega}_i$: computational domain is decomposed into non-overlapping subdomain blocks

$$\Gamma_{ij} = \partial\Omega_i \cap \partial\Omega_j, \quad \Gamma = \cup_{i,j=1}^{n_b} \Gamma_{ij}, \quad \Gamma_i = \partial\Omega_i \cap \Gamma = \partial\Omega_i \setminus \partial\Omega$$

On each block Ω_i : $\mathcal{T}_{h,i}$ – finite element partition

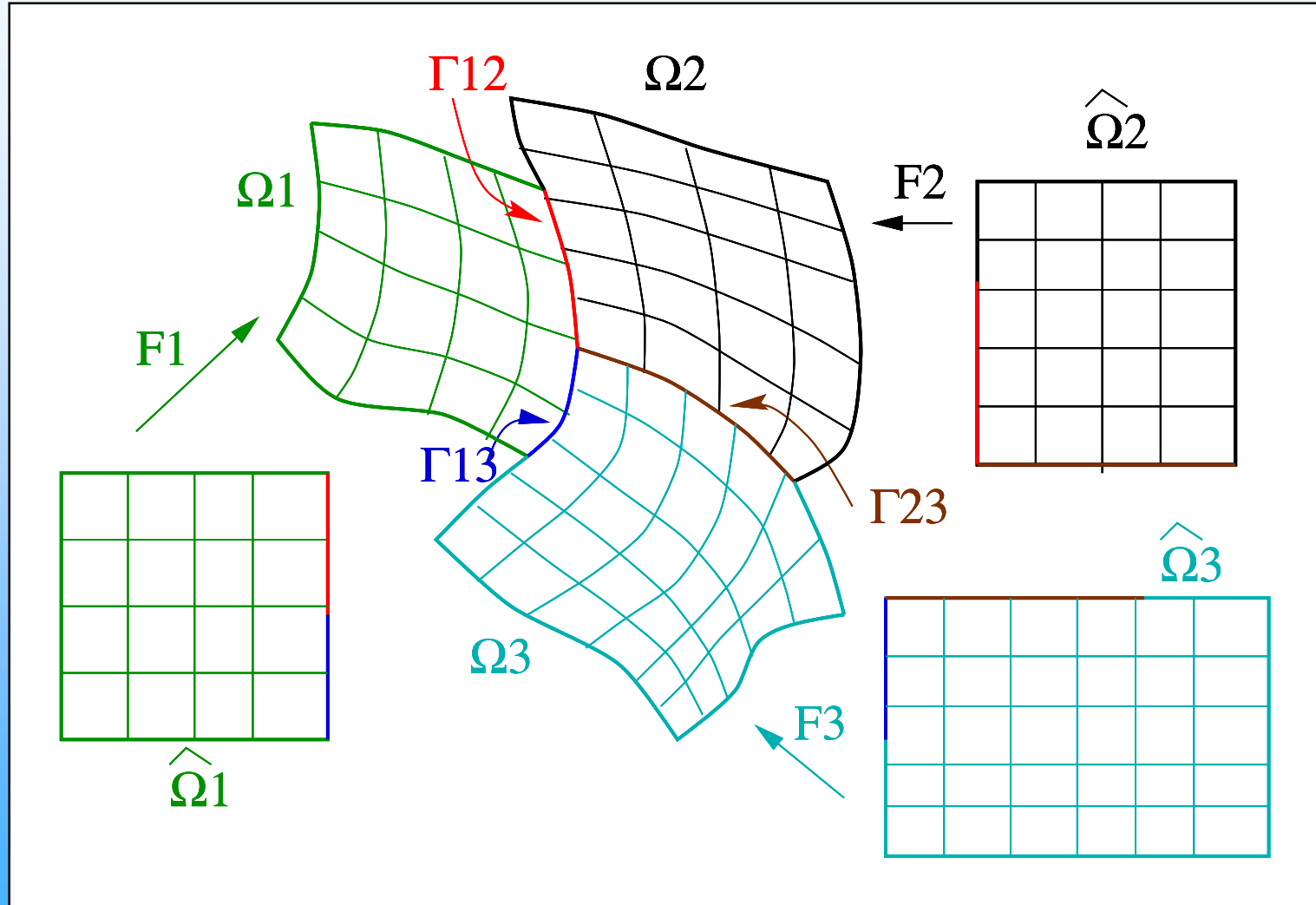
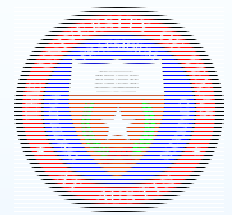
$\mathbf{V}_{h,i} \times W_{h,i} \subset H(\text{div}; \Omega_i) \times L^2(\Omega_i)$ – MFE spaces on $\mathcal{T}_{h,i}$

On each interface $\Gamma_{i,j}$: $\mathcal{T}_{H,i,j}$ – interface finite element grid

$M_{H,i,j} \subset L^2(\Gamma_{i,j})$ – mortar space on $\mathcal{T}_{H,i,j}$

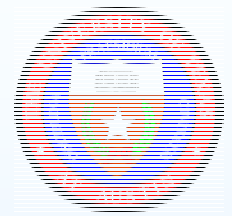
$$\mathbf{V}_h = \bigoplus_{i=1}^{n_b} \mathbf{V}_{h,i}, \quad W_h = \bigoplus_{i=1}^{n_b} W_{h,i}, \quad M_H = \bigoplus_{1 \leq i < j \leq n_b} M_{H,i,j}$$

Mortar Domain Decomposition





Equations for Multiphase Flow



Mass balance in each sub-domain:
$$\frac{\partial(\varphi \rho_\alpha S_\alpha)}{\partial t} + \nabla \cdot (\rho_\alpha \mathbf{u}_\alpha) = q_\alpha$$

Darcy's law (constitutive equation):
$$\mathbf{u}_\alpha = -\frac{k_{r\alpha}(S_\alpha)K}{\mu_\alpha}(\nabla p_\alpha - \rho_\alpha g \nabla D)$$

Saturation constraint:
$$\sum_{\alpha} S_\alpha = 1$$

Capillary pressure relation:
$$p_c(S_w) = p_n - p_w$$

Continuity: On each interface $\Gamma_{i,j}$ physically meaningful BC applied:

$$p_\alpha|_{\Omega_i} = p_\alpha|_{\Omega_j} \quad [\mathbf{u}_\alpha \cdot \mathbf{n}]_{i,j} \equiv \mathbf{u}_\alpha|_{\Omega_i} \cdot \mathbf{n}_i + \mathbf{u}_\alpha|_{\Omega_j} \cdot \mathbf{n}_j = 0$$

Introduce a pressure gradient term to avoid inverting $k_{r\alpha}$:

$$\tilde{\mathbf{u}}_\alpha = -K/\mu_\alpha(\nabla p_\alpha - \rho_\alpha g \nabla D), \quad \mathbf{u}_\alpha = k_{r\alpha}(S_\alpha)\tilde{\mathbf{u}}_\alpha$$

In a **backward Euler multi-block**, we seek $\mathbf{u}_{\alpha,h}^n|_{\Omega_i} \in \mathbf{V}_{h,i}$,

$$\tilde{\mathbf{u}}_{\alpha,h}^n|_{\Omega_i} \in \tilde{\mathbf{V}}_{h,i}, \quad p_h^n|_{\Omega_i} \in W_{h,i}, \quad S_h^n|_{\Omega_i} \in W_{h,i}, \quad p_H^n|_{\Gamma_{i,j}} \in M_{H,i,j},$$

$$S_H^n|_{\Gamma_{i,j}} \in M_{H,i,j} \quad \text{for } 1 \leq i < j \leq n_b, \text{ such that:}$$

$$\left(\frac{\Delta(\varphi \rho_{\alpha,h} S_{\alpha,h})^n}{\Delta t^n}, w \right)_{\Omega_i} + (\nabla \cdot \rho_{\alpha,h}^n \mathbf{u}_{\alpha,h}^n, w)_{\Omega_i} = (q_\alpha^n, w)_{\Omega_i}, \quad w \in W_{h,i}$$

$$\left(\left(\frac{K}{\mu_{\alpha,h}} \right)^{-1} \tilde{\mathbf{u}}_{\alpha,h}^n, \mathbf{v} \right)_{\Omega_i} = (p_{\alpha,h}^n, \nabla \cdot \mathbf{v})_{\Omega_i} - \langle p_{\alpha,H}^n, \mathbf{v} \cdot \mathbf{n}_i \rangle_{\Gamma_i}$$

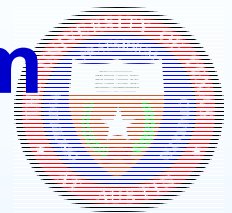
$$+ (\rho_{\alpha,h}^n g \nabla D, \mathbf{v})_{\Omega_i}, \quad \mathbf{v} \in \mathbf{V}_{h,i}$$

$$(\mathbf{u}_{\alpha,h}^n, \tilde{\mathbf{v}})_{\Omega_i} = (k_{r\alpha,h}^n \tilde{\mathbf{u}}_{\alpha,h}^n, \tilde{\mathbf{v}})_{\Omega_i}, \quad \tilde{\mathbf{v}} \in \tilde{\mathbf{V}}_{h,i}$$

$$\langle [\mathbf{u}_{\alpha,h}^n \cdot \mathbf{n}]_{i,j}, \zeta \rangle_{\Gamma_{i,j}} = 0, \quad \zeta \in M_{H,i,j}$$



Reduction to an Interface Problem



Let $\mathbf{M}_H = M_H \times M_H$. Define

$$b^n(\psi, \eta) = \sum_{1 \leq i < j \leq n_b} \sum_{\alpha} \int_{\Gamma_{i,j}} \left[\rho_{\alpha,h}^n \mathbf{u}_{\alpha,h}^n(\psi) \cdot \mathbf{n} \right]_{ij} \eta_{\alpha} ds,$$

where $\psi = (p_{w,H}^n, S_{w,H}^n) \in \mathbf{M}_H$, $\eta = (\eta_w, \eta_w) \in \mathbf{M}_H$

Define the **non-linear interface operator** $\mathcal{B}^n : \mathbf{M}_H \rightarrow \mathbf{M}_H$ by

$$\langle \mathcal{B}^n \psi, \eta \rangle = b^n(\psi, \eta), \quad \forall \eta \in \mathbf{M}_H$$

Then $(\psi, p_{\alpha,h}^n(\psi), S_{\alpha,h}^n(\psi), \mathbf{u}_{\alpha,h}^n(\psi))$ solves the multiphase flow equations when $\mathcal{B}^n(\psi) = 0$

Interface problem is solved by “**inexact Newton-GMRES**” scheme

Mass balance of species i in phase α :

$$\frac{\partial(\varphi c_{i\alpha} S_\alpha)}{\partial t} + \nabla \cdot (c_{i\alpha} \mathbf{u}_\alpha - \varphi S_\alpha \mathbf{D}_{i\alpha} \nabla c_{i\alpha}) = r(c_{i\alpha})$$

$$\mathbf{D}_{i\alpha} \nabla c_{i\alpha} \cdot \mathbf{n} = 0$$

Diffusion-Dispersion tensor $\mathbf{D}_{i\alpha} = \mathbf{D}_{i\alpha}^{\text{diff}} + \mathbf{D}_{i\alpha}^{\text{hyd}}$:

Molecular diffusion: $\mathbf{D}_{i\alpha}^{\text{mol}} = \tau_\alpha d_{m,i\alpha} \mathcal{I}$

Physical dispersion: $\varphi S_\alpha \mathbf{D}_{i\alpha}^{\text{hyd}} = d_{t,\alpha} |\mathbf{u}_\alpha| \mathcal{I} + (d_{l,\alpha} - d_{t,\alpha}) \frac{\mathbf{u}_\alpha \mathbf{u}_\alpha^T}{|\mathbf{u}_\alpha|}$

Source term: $r(c_{i\alpha}) = r_{i\alpha}^I + \varphi S_\alpha r_{i\alpha}^C + q_{i\alpha}$,

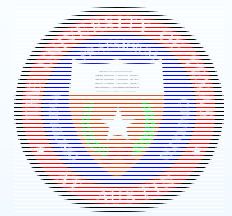
where $r_{i\alpha}^I$ is influx/efflux from other phases,

$r_{i\alpha}^C$ is chemical rate of decay

$q_{i\alpha}$ is a source (or sink) term



Phase-Summed Equations



Assume an equilibrium partitioning of species between phases:

$$c_{i\alpha} = \theta_{i\alpha} c_{i\alpha_0}$$

Sum over all phases for a given species:

$$\frac{\partial(\varphi_i^* c_{iw})}{\partial t} + \nabla \cdot (c_{iw} \mathbf{u}_i^* - \mathbf{D}_i^* \nabla c_{iw}) = r_i^*(\mathbf{c}_w)$$

$$\mathbf{D}_{iw} \nabla c_{iw} \cdot \mathbf{n} = 0$$

$$\varphi_i^* = \varphi \sum_{\alpha} \theta_{i\alpha} S_{\alpha}$$

$$\mathbf{u}_i^* = \sum_{\alpha} \theta_{i\alpha} \mathbf{u}_{\alpha}$$

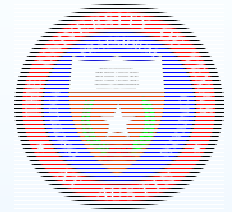
$$\mathbf{D}_i^* = \varphi \sum_{\alpha} S_{\alpha} \theta_{i\alpha} \mathbf{D}_{i\alpha}$$

$$r_i^*(\mathbf{c}_w) = \varphi \sum_{\alpha} r_{i\alpha}^C - r_{iR} + \sum_{\alpha} q_{i\alpha}$$

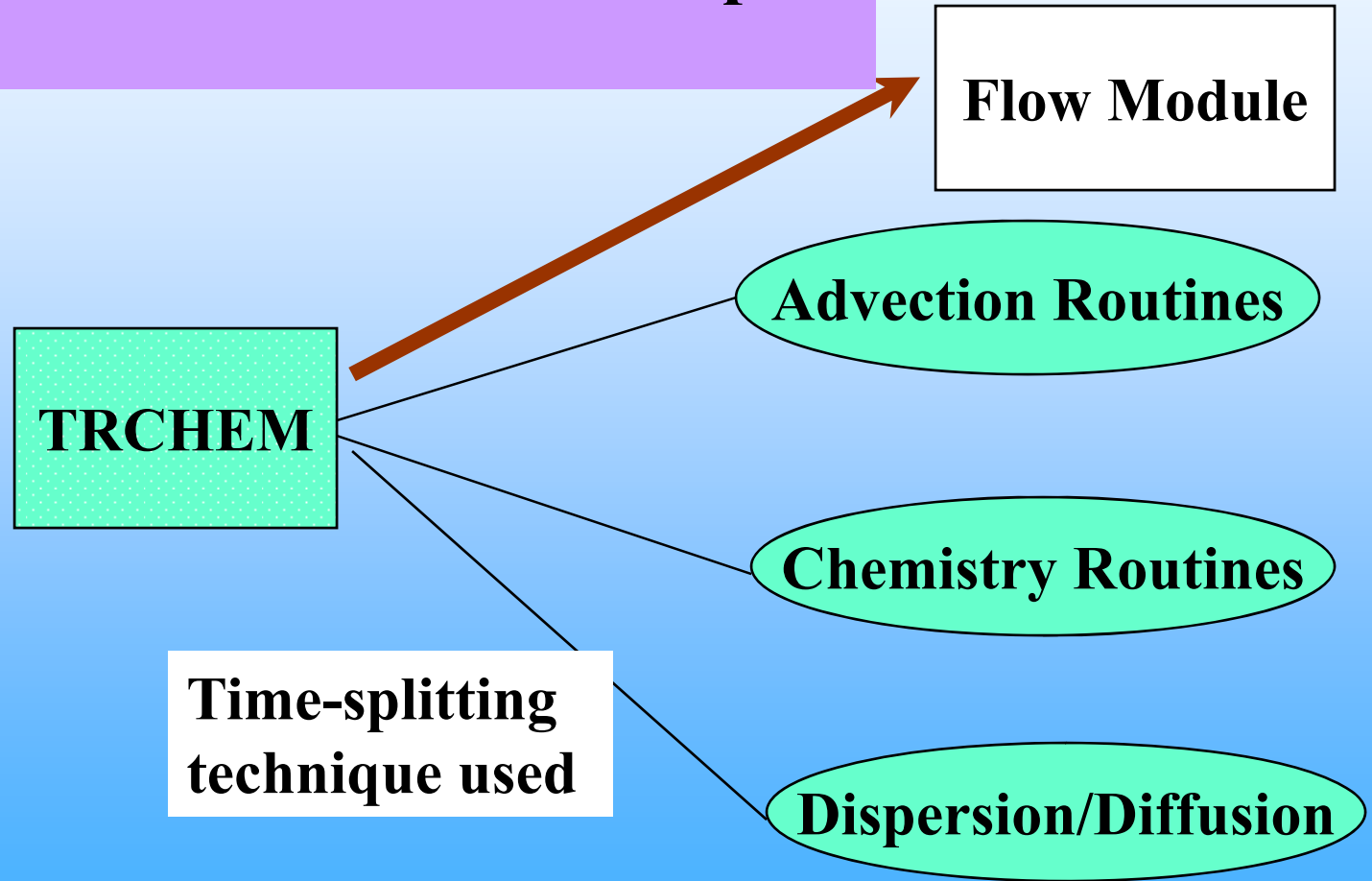
Note: $\sum_{\alpha} r_{i\alpha}^I + r_{iR} = 0$, where r_{iR} is the influx/efflux of species i into the stationary phase



IPARS-TRCHEM Structure



**IPARS TRCHEM =
Flow and Reactive Transport**



$$\left(\frac{\partial \varphi_i^* c_{iw}}{\partial t}, w \right)_{\Omega_j} + (\nabla \cdot (c_{iw} \mathbf{u}_i^*), w)_{\Omega_j} = \left(\sum_{\alpha} q_{i\alpha}, w \right)_{\Omega_j}, w \in W_j$$

Solved using a **Godunov** scheme

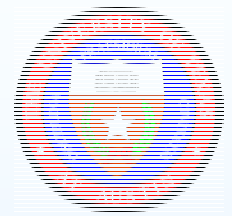
First order Godunov scheme

Let $T_i^m = \varphi_i^{*,m} c_{h,iw}^m$, solve for \bar{T}_i from

$$\left(\frac{\bar{T}_i - T_i^m}{\Delta \tau^{m+1}}, w \right)_{\Omega_j} + \sum_{E \in \mathcal{T}_{h,j}} \langle c_{h,iw}^{m,\text{upw}} \mathbf{u}_{h,i}^{*,m+1/2} \cdot \mathbf{n}_E, w \rangle_{\partial E} = \left(\sum_{\alpha} q_{i\alpha}, w \right)_{\Omega_j}$$



Chemical Reaction



Define $\Phi(t) \equiv \text{diag}\{\varphi_i^*(t)\}$, $\mathbf{T} = \mathbf{T}(t) \equiv \Phi(t)\mathbf{c}_w$, and

$$r_i^{*,C}(\mathbf{T}) \equiv \varphi \sum_{\alpha} r_{i\alpha}^C(\Phi^{-1}(t)\mathbf{T}) \quad \text{Then} \quad \frac{\partial \mathbf{T}_i}{\partial t} = r_i^{*,C}(\mathbf{T})$$

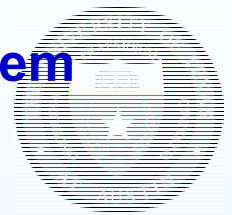
Solved by explicit **ODE integration using Runge-Kutta**

Second order Runge-Kutta scheme

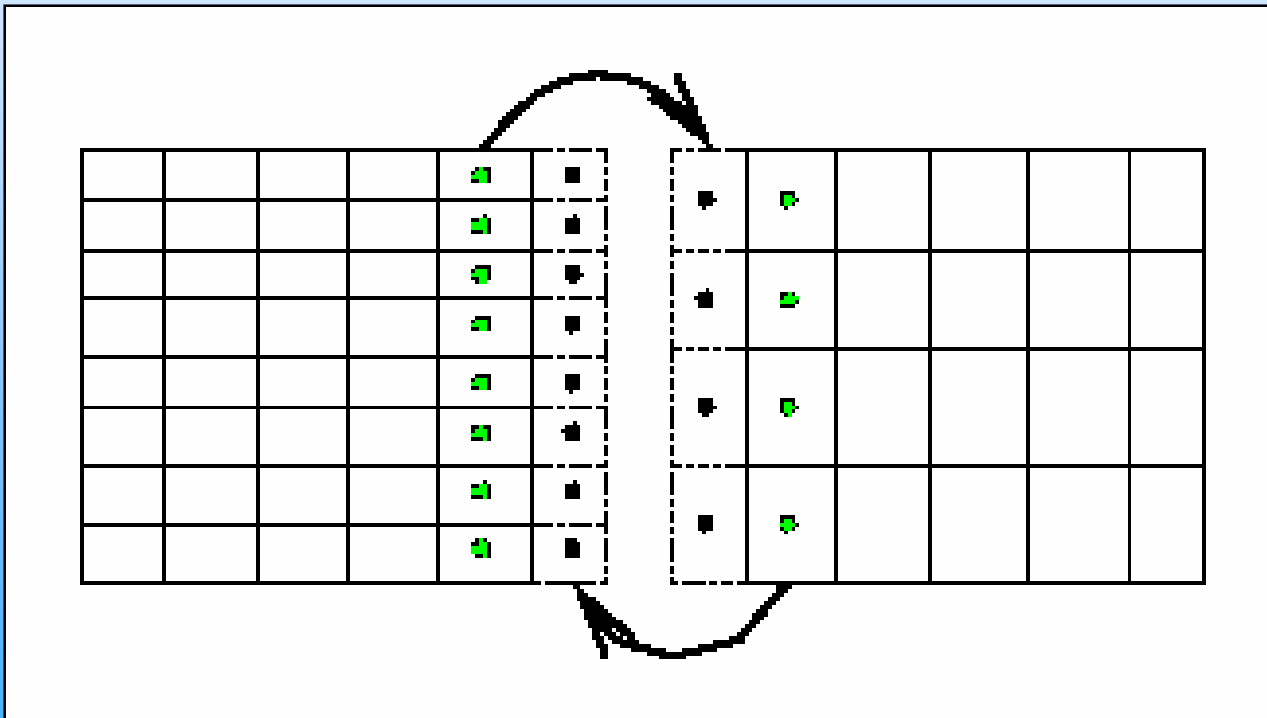
$$k_{1,i} = \Delta\tau^{m+1} r_i^{*,C}(\bar{\mathbf{T}})$$

$$k_{2,i} = \Delta\tau^{m+1} r_i^{*,C}\left(\bar{\mathbf{T}} + \frac{1}{2}\mathbf{k}_1\right)$$

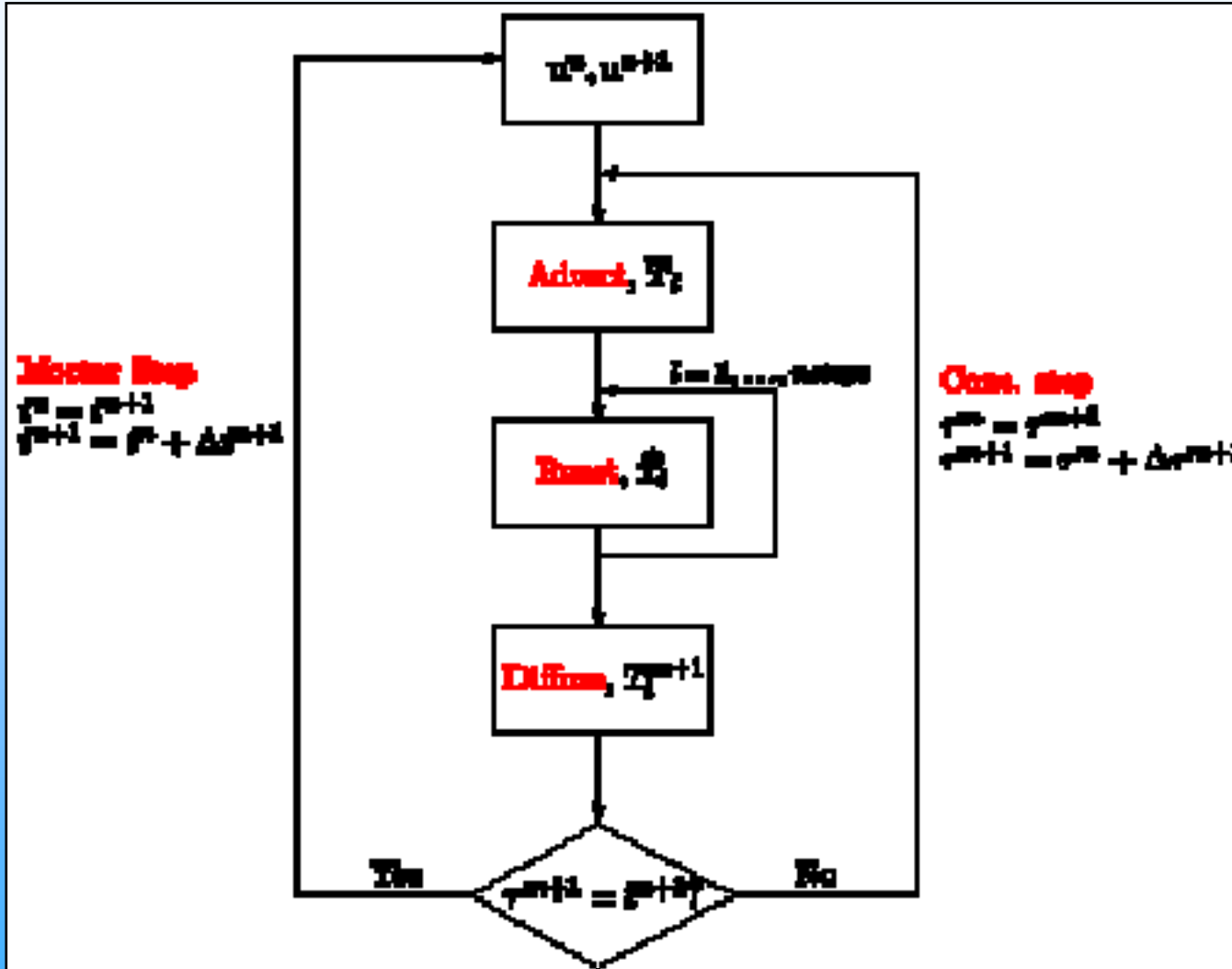
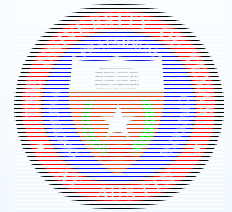
$$\hat{T}_i = \bar{T} + k_{2,i}$$



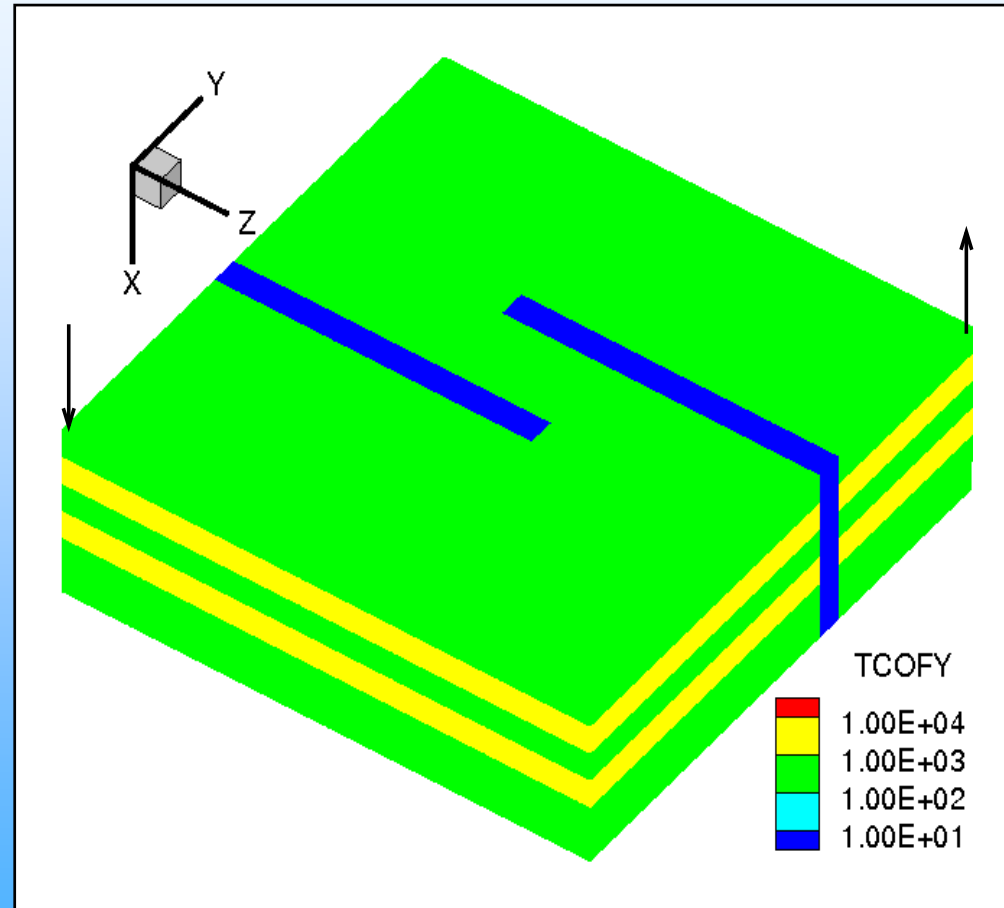
$\mathcal{P}_j : L^2(\Gamma_j) \rightarrow L^2(\Gamma_k)$ is an L^2 -orthogonal proj. s.t. $\forall \phi \in L^2(\Gamma_j)$
 $\langle \phi - \mathcal{P}_j \phi, \mathbf{v} \cdot \mathbf{n}_j \rangle_{\Gamma_{k,j}} = 0, \forall \mathbf{v} \in \mathbf{V}_{h,i}, \forall k$ such that $\bar{\Omega}_k \cap \bar{\Omega}_j \neq \emptyset$



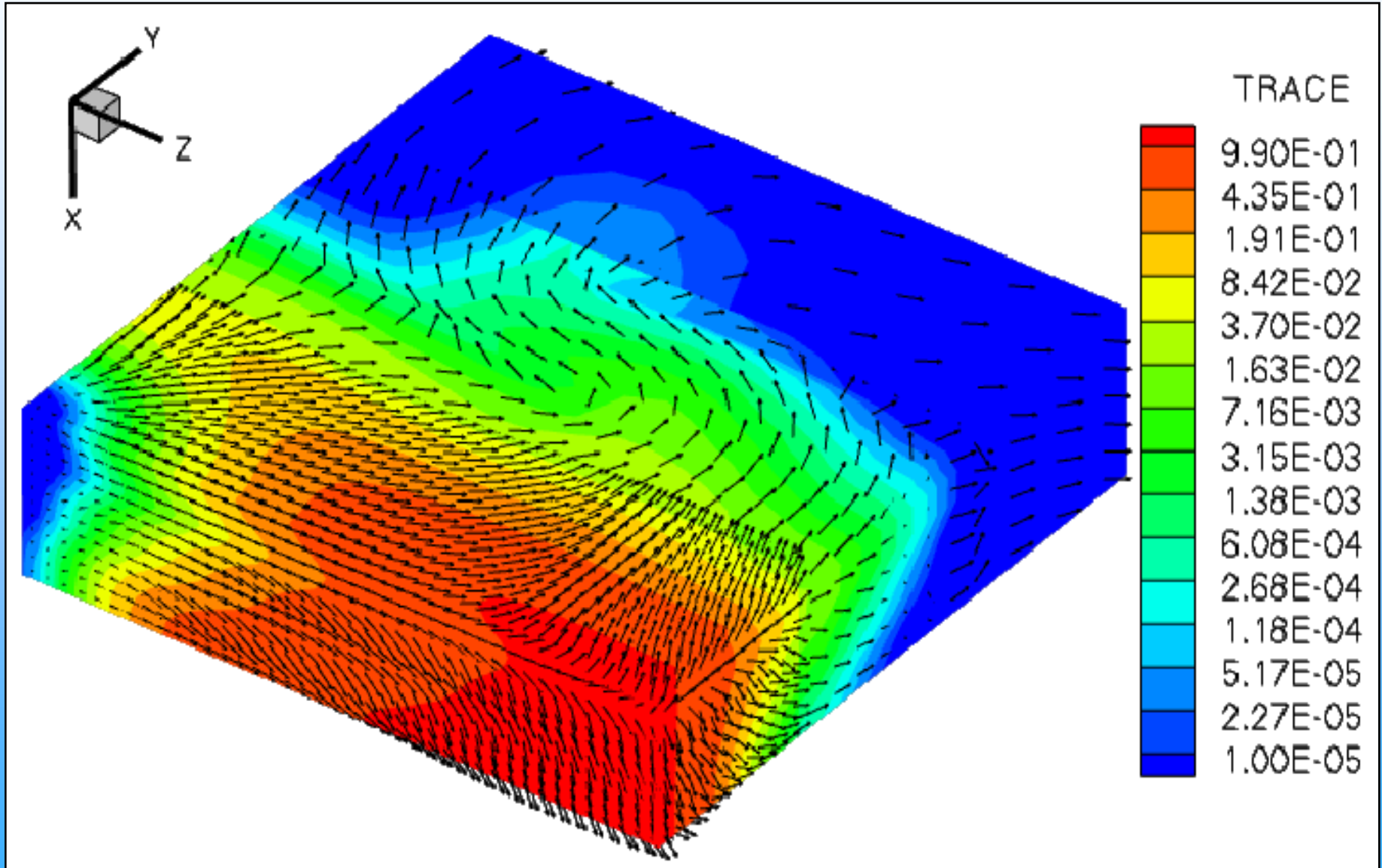
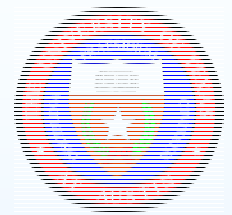
Algorithm



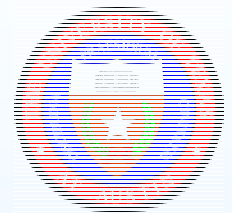
- ◆ Bio-remediation of NAPL using microbes
- ◆ Advection-Diffusion-Reaction
- ◆ Discontinuous permeability field with barriers
- ◆ Two flowing phases - quarter-five spot
- ◆ External BC: no-flow and zero diffusive flux
- ◆ IC: NAPL, microbes occupy $0 < y < 40$ ft and O_2 , N_2 occupy $40 < y < 400$ ft.
- ◆ Domain: 20 ft x 400 ft x 400 ft
- ◆ Reference case: $NX=20$, $NY=40$, $NZ=40$



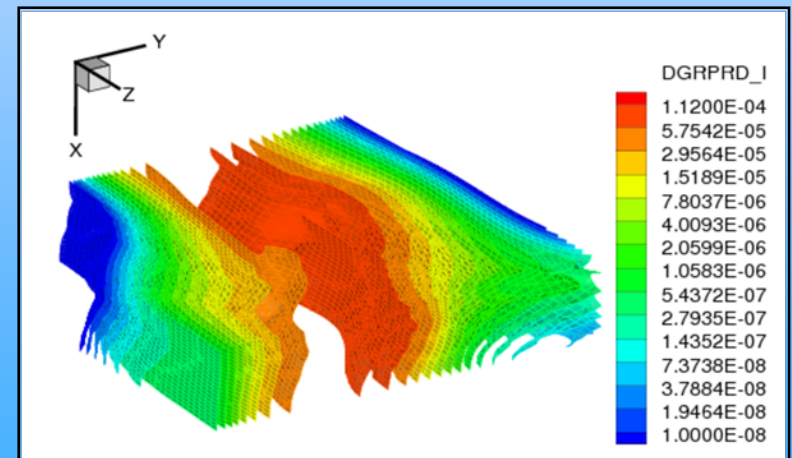
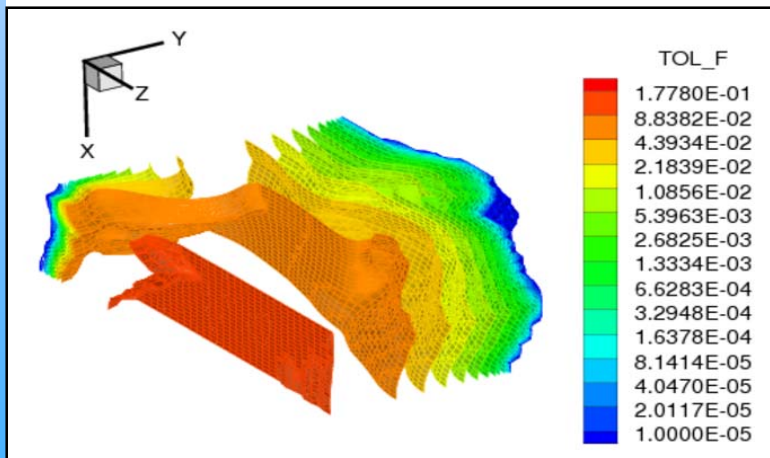
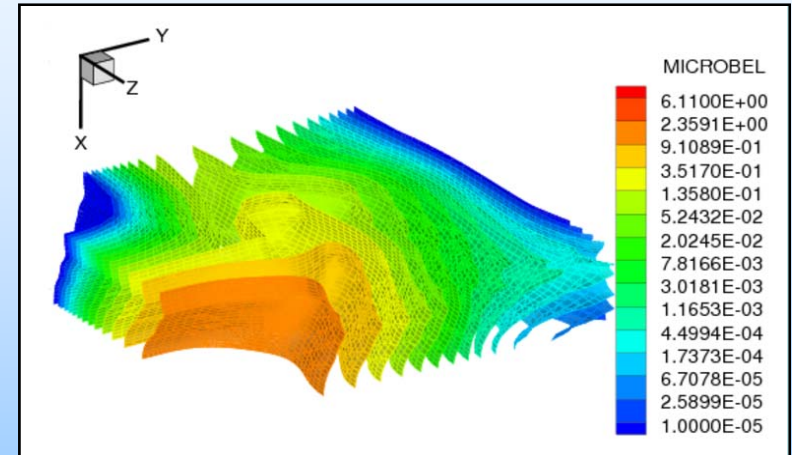
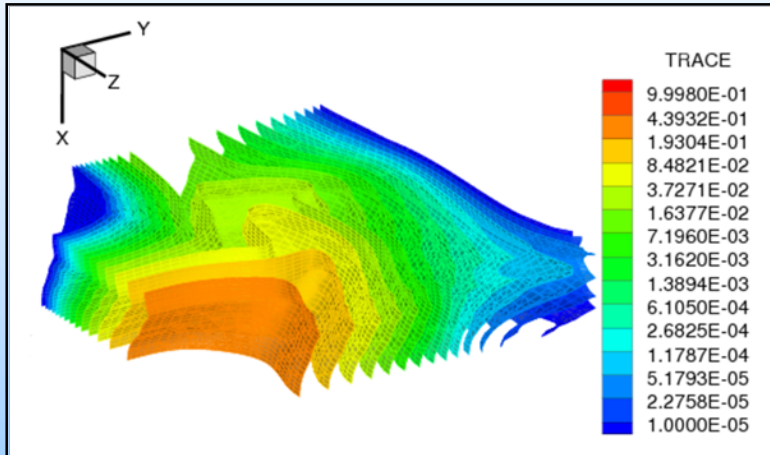
Flow Pattern in Multi-block



Reference Solution

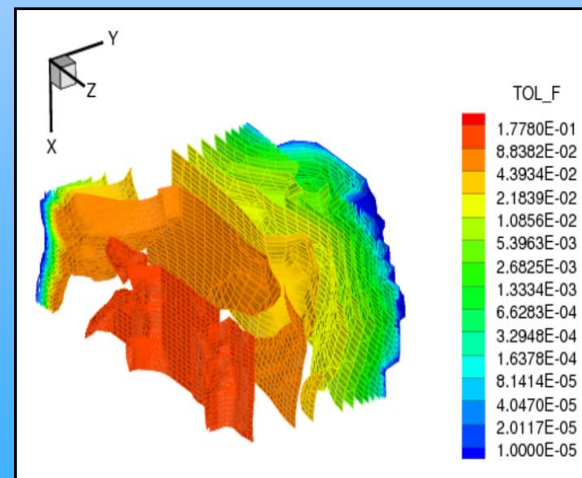
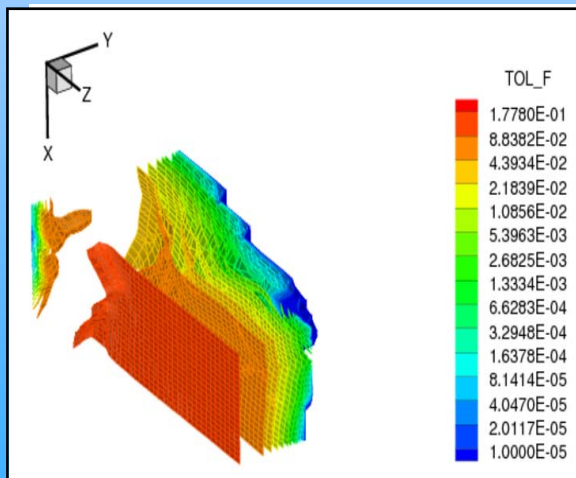
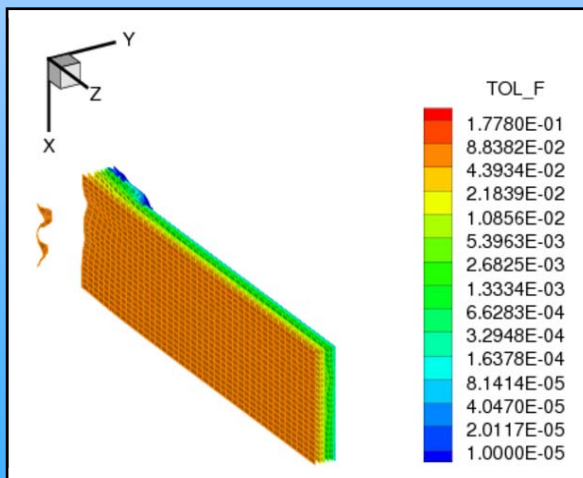
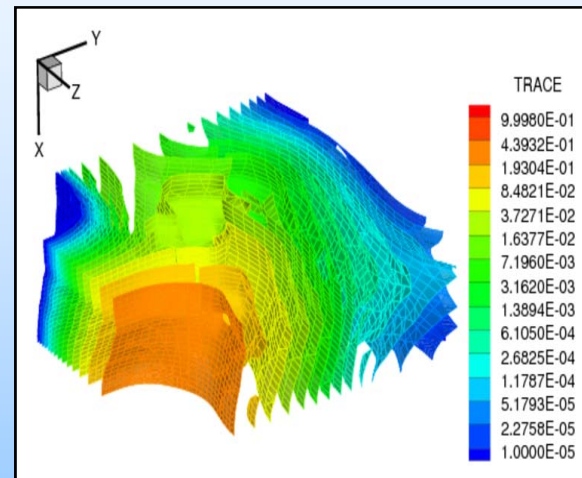
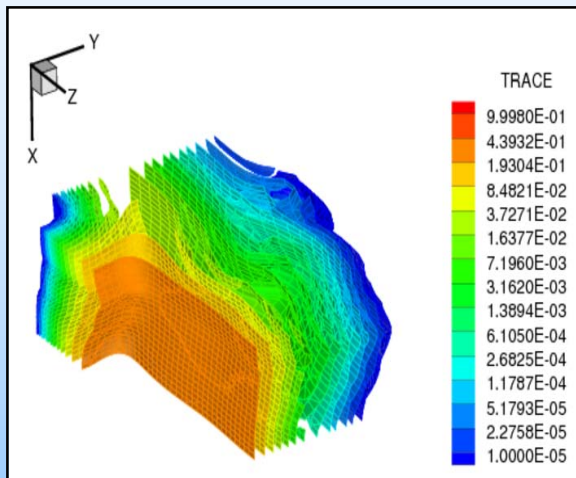
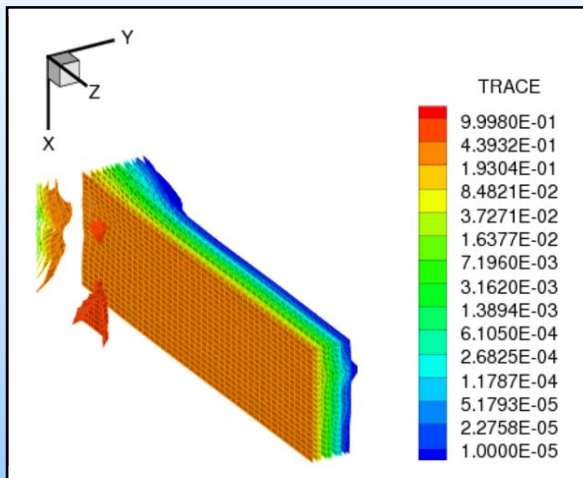


Concentrations of tracer, NAPL, microbes and bio-degraded product at 100 days

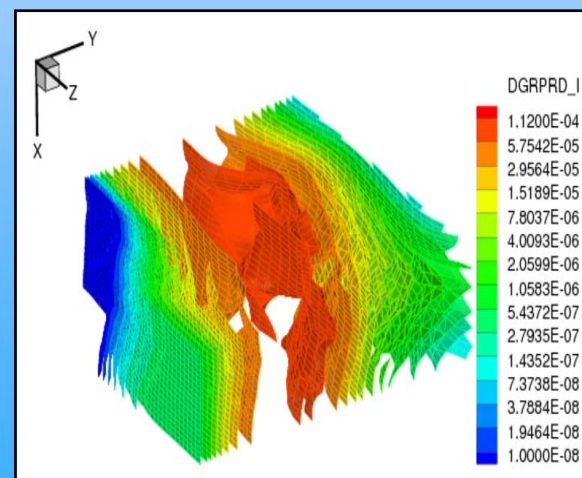
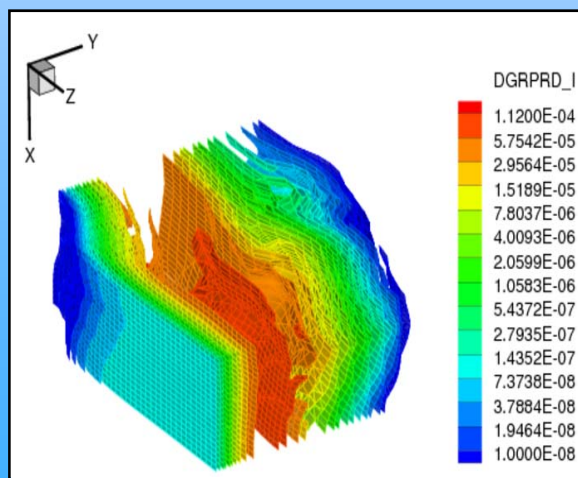
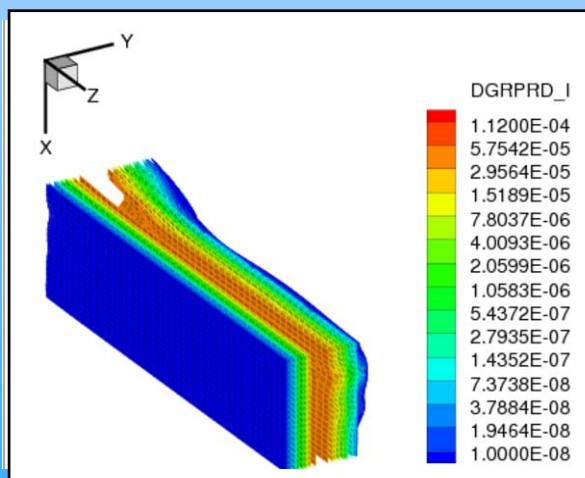
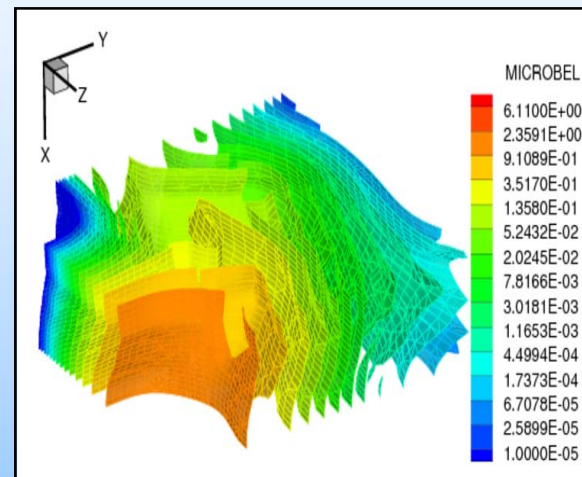
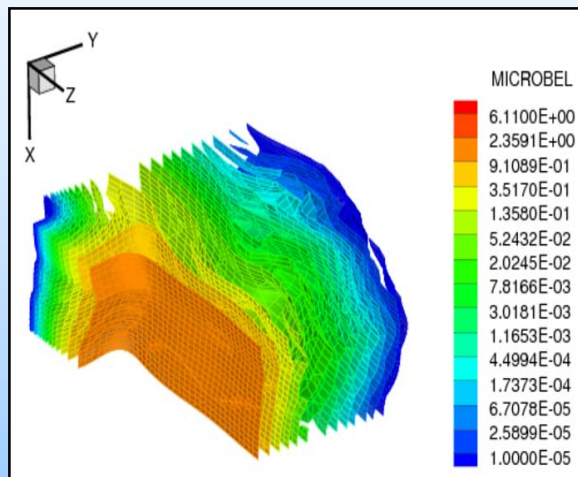
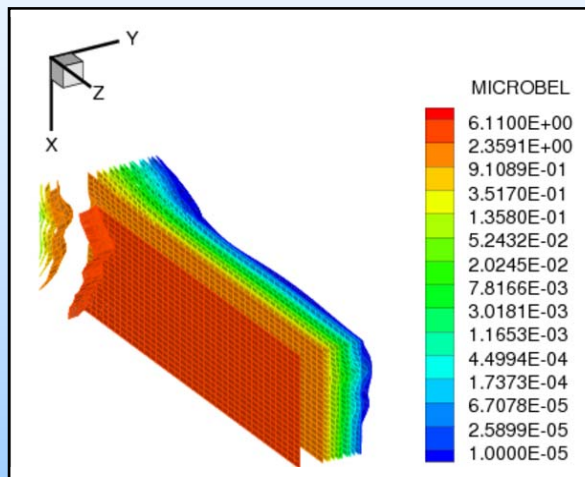


Comparison to Mortar Scheme

Tracer & NAPL concentrations at 5, 50, 100 days

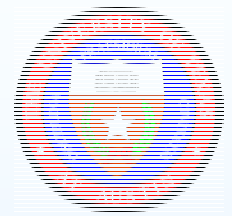


Microbe & product concentrations at 5, 50, 100 days



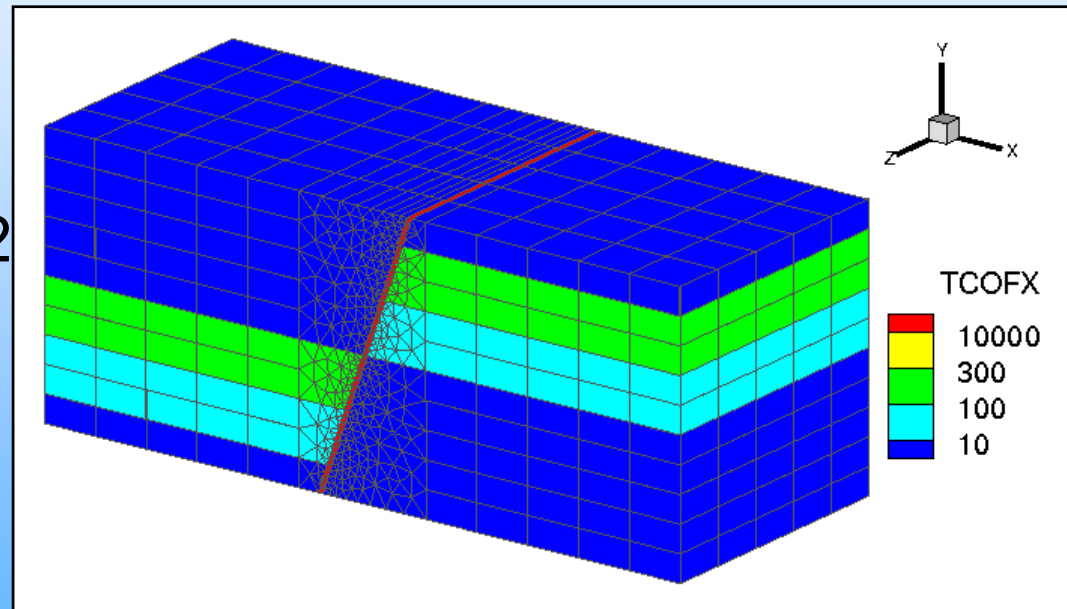


Multinumeric Extensions

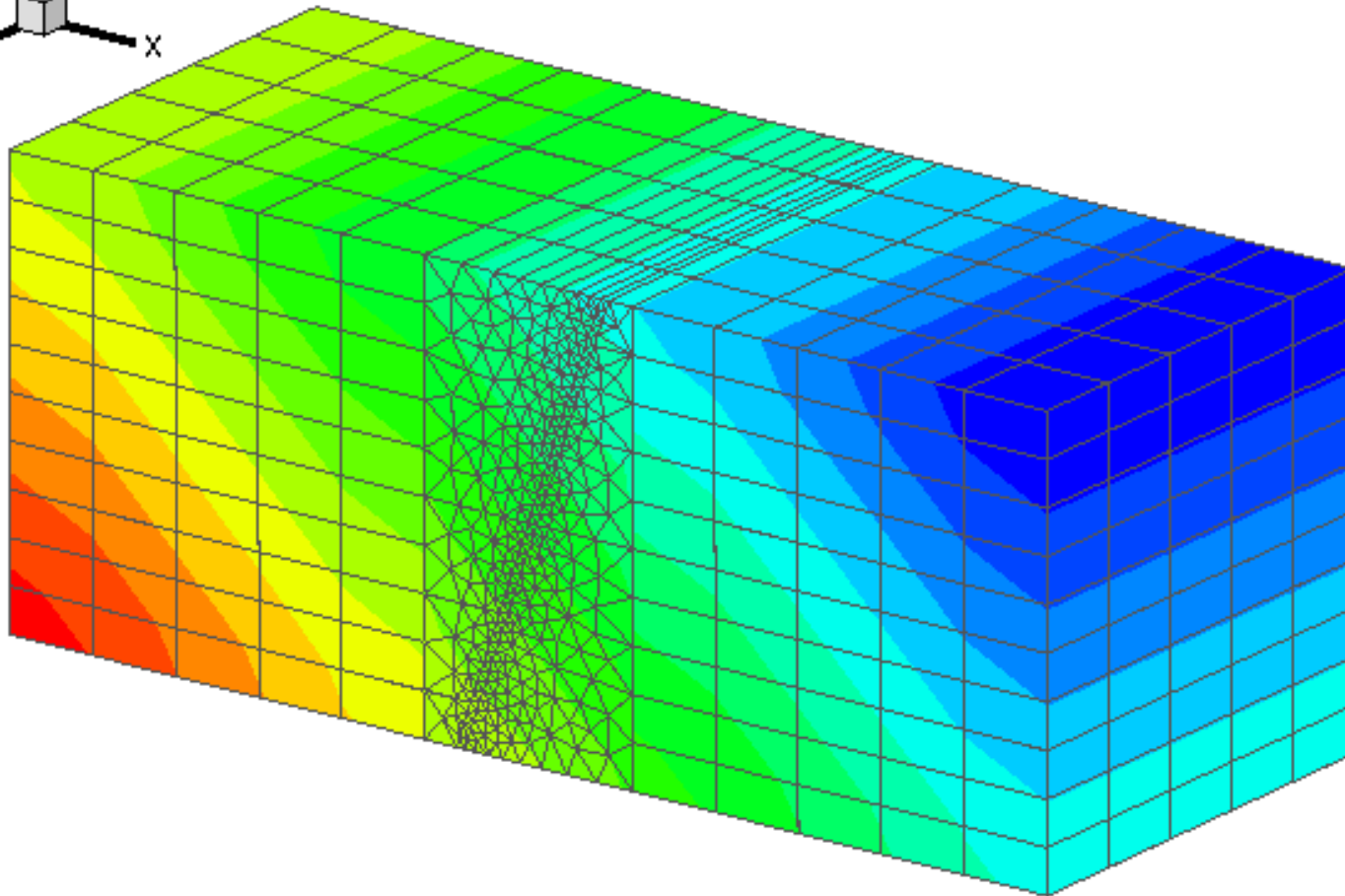
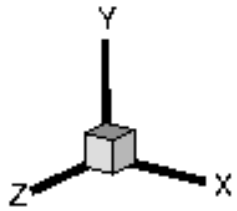
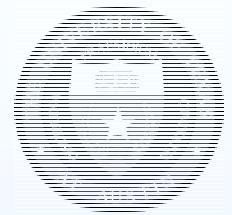


- ◆ DG and Mixed FEM can be combined for treating flow using mortar spaces
- ◆ DG is applicable for both flow and transport on non-matching grids
- ◆ Examples for single-phase slightly compressible flow follow

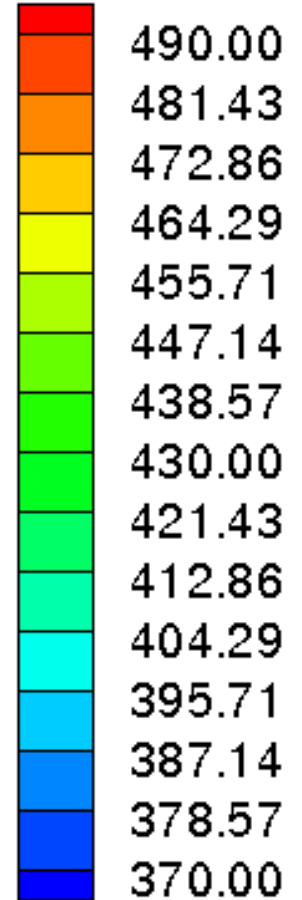
- ◆ 250 x 100 x 100 ft
- ◆ 2 ft wide fault: 10000 mD, $\phi=0.01$
- ◆ 4 geological layers: 10, 100, 300, 10 mD, $\phi=0.2$
- ◆ BC:
 - 500 psi at $x=0$
 - 400 psi at $x=250$,
 - noflow o.w.
- ◆ $r=2$, $k=0$ (RT0), $m=0$



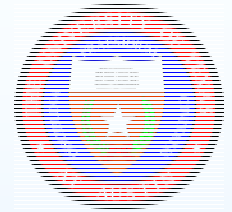
3 blocks with a fault : Solution



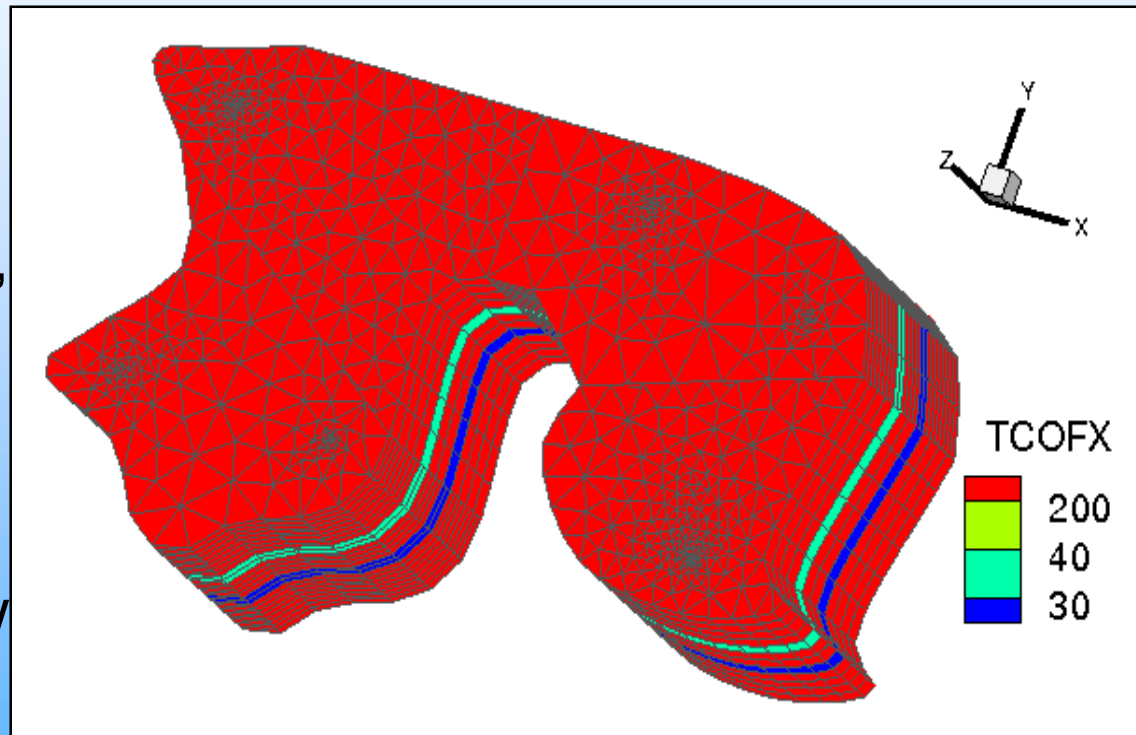
PRES



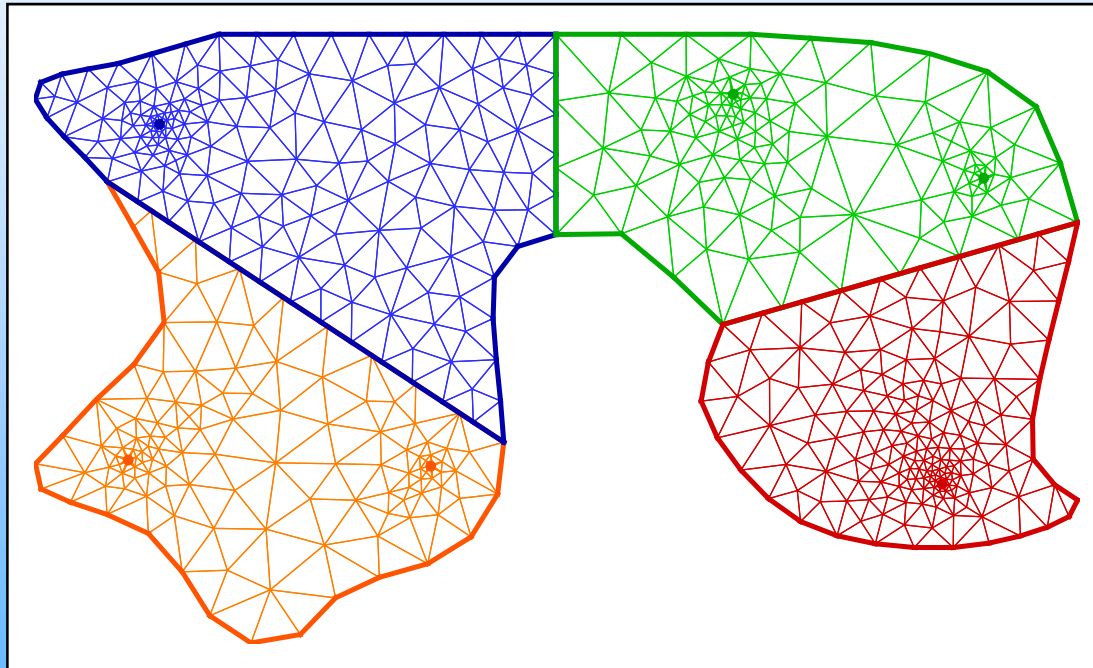
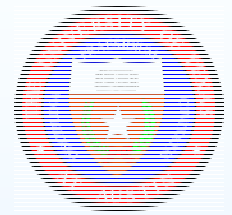
DG-DG, Oxbow problem



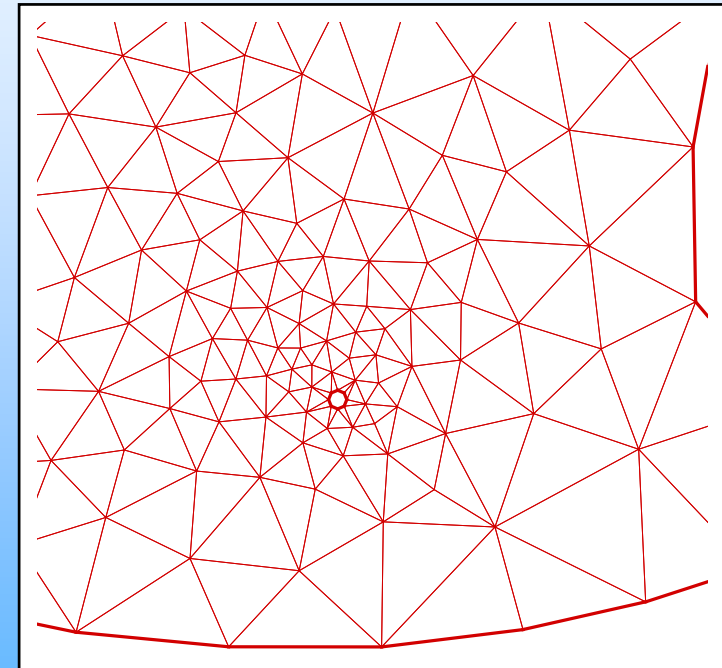
- ◆ 4 blocks with 6 wells
- ◆ 900 x 500 x 24 ft
- ◆ 1 production, 5 injection wells
- ◆ $K_{xx} = K_{yy} = \{200, 30, 40\}$,
 $K_{zz} = \{25, 5, 3\}$,
 $\phi = \{0.22, 0.08, 0.09\}$
- ◆ BC: $P_{inj} = 700$ psi,
 $P_{prod} = 500$ psi, noflow
on the outer bdry
- ◆ nonmatching grids,
 $r=2$, $m=1$



Unstructured Mesh



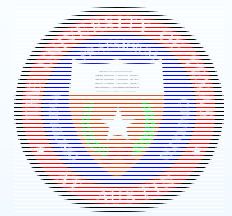
Top view, 4 blocks



Magnified grid around well



Linear Elasticity Problem



Find $u \in H^1(\Omega)$ s.t.

$$-\nabla \cdot \boldsymbol{\sigma}(u) = f \quad \text{in } \Omega$$

$$u = u_D \quad \text{on } \Gamma_D$$

$$\boldsymbol{\sigma}(u)\mathbf{n} = t_N \quad \text{on } \Gamma_N$$

$$\boldsymbol{\sigma}(u) = \lambda \nabla \cdot u \mathbf{I} + 2\mu \boldsymbol{\varepsilon}(u) \quad \text{- anisotropic Hooke's law}$$

$$\boldsymbol{\varepsilon}(u) = \frac{1}{2} (\nabla u + \nabla u^T) \quad \text{- kinematic equation}$$

u : displacement

$\boldsymbol{\varepsilon}$: linearized strain tensor

$\boldsymbol{\sigma}$: Cauchy stress

$\lambda > 0, \mu > 0$: Lamé parameters

$$\Omega = \Omega_1 \cup \Omega_2 \cup \Gamma_{12}$$

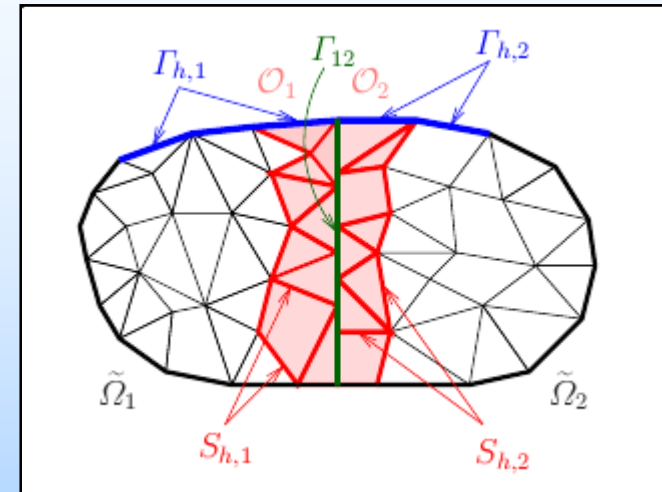
Find u with $u|_{\Omega_i} \in H^1(\Omega_i)$ s.t.

On each block Ω_i :

$$-\nabla \cdot \boldsymbol{\sigma}(u) = f \quad \text{in } \Omega_i$$

$$u = u_D \quad \text{on } \Gamma_{D_i} = \partial\Omega_i \cap \Gamma_D$$

$$\boldsymbol{\sigma}(u)\mathbf{n} = t_N \quad \text{on } \Gamma_{N_i} = \partial\Omega_i \cap \Gamma_N$$

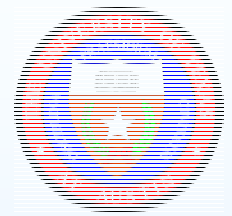


On the interface Γ_{12} :

$$[u] = 0, \quad [\boldsymbol{\sigma}(u)]n_1 = 0, \quad \text{on } \Gamma_{12} \quad : \text{ transmission conditions}$$



Discrete Spaces



$\mathcal{T}_h(\Omega_i)$ – a conforming partition of Ω_i , $i = 1, 2$

\mathcal{E}_H – mortar finite element partition on Γ_{12} , independent of interior meshes

$$X_{h,i} = \{ \mathbf{v}_{h,i} \in L^2(\Omega_i) : \mathbf{v}_{h,i}|_{\tilde{\Omega}_i} \in H^1(\tilde{\Omega}_i), \forall E \in \mathcal{T}_{h,i}, \mathbf{v}_{h,i}|_E \in \mathbf{IP}_k(E) \}$$

$$\Lambda_H = \{ \boldsymbol{\lambda}_H \in L^2(\Gamma_{12}) : \forall \tau \in \mathcal{E}_H, \boldsymbol{\lambda}_H|_{\tau} \in \mathbf{IP}_l(E) \}$$

$$\forall \mathbf{v}_h \in X_h, |\mathbf{v}_h|_{X_h} = \left(\sum_{i=1}^2 |\mathbf{v}_{h,i}|_{h,i}^2 \right)^{1/2}$$

$$\begin{aligned} |\mathbf{v}_{h,i}|_{h,i}^2 &= \lambda \left(\|\operatorname{div} \mathbf{v}_{h,i}\|_{L^2(\tilde{\Omega}_i)}^2 + \sum_{E \in \mathcal{O}_i} \|\operatorname{div} \mathbf{v}_{h,i}\|_{L^2(E)}^2 \right) \\ &\quad + 2\mu \left(\|\varepsilon(\mathbf{v}_{h,i})\|_{L^2(\tilde{\Omega}_i)}^2 + \sum_{E \in \mathcal{O}_i} \|\varepsilon(\mathbf{v}_{h,i})\|_{L^2(E)}^2 \right) \end{aligned}$$

$$\begin{aligned}
 & \sum_{i=1}^2 \left(\int_{\Omega_i} \boldsymbol{\sigma}(\mathbf{u}_i) : \boldsymbol{\epsilon}(\mathbf{v}_i) - \int_{\Gamma_{D_i}} (\boldsymbol{\sigma}(\mathbf{u}_i) \mathbf{n}_{\Omega} \cdot \mathbf{v}_i + s_D \boldsymbol{\sigma}(\mathbf{v}_i) \mathbf{n}_{\Omega} \cdot \mathbf{u}_i) \right. \\
 & \quad - \int_{\Gamma_{12}} (\boldsymbol{\sigma}(\mathbf{u}_i) \mathbf{n}_i \cdot \mathbf{v}_i - \boldsymbol{\sigma}(\mathbf{v}_i) \mathbf{n}_i \cdot \mathbf{u}_i) \\
 & \quad \left. + (\lambda + 2\mu) \left(\sum_{\gamma \in \Gamma_{h,i}} \frac{\sigma_{\gamma}}{h_{\gamma}} \int_{\gamma} \mathbf{u}_i \cdot \mathbf{v}_i + \sum_{\tau \in \mathcal{E}_H} \frac{\sigma_{\tau}}{H_{\tau}} \int_{\tau} \mathbf{u}_i \cdot \mathbf{v}_i \right) \right) \\
 & = \int_{\Omega} \mathbf{f} \cdot \mathbf{v} + \int_{\Gamma_N} \mathbf{t}_N \cdot \mathbf{v} \\
 & \quad - \sum_{i=1}^2 \left(s_D \int_{\Gamma_{D_i}} \boldsymbol{\sigma}(\mathbf{v}_i) \mathbf{n}_{\Omega} \cdot \mathbf{u}_D - (\lambda + 2\mu) \sum_{\gamma \in \Gamma_{h,i}} \frac{\sigma_{\gamma}}{h_{\gamma}} \int_{\gamma} \mathbf{u}_D \cdot \mathbf{v}_i \right) \\
 & \quad + \sum_{i=1}^2 \left(\int_{\Gamma_{12}} \boldsymbol{\sigma}(\mathbf{v}_i) \mathbf{n}_i \cdot \boldsymbol{\lambda} + (\lambda + 2\mu) \sum_{\tau \in \mathcal{E}_H} \frac{\sigma_{\tau}}{H_{\tau}} \int_{\tau} \boldsymbol{\lambda} \cdot \mathbf{v}_i \right), \quad \forall \mathbf{v}
 \end{aligned}$$

$$\int_{\Gamma_{12}} [\boldsymbol{\sigma}(\mathbf{u})]_{12} \mathbf{n}_{12} \cdot \boldsymbol{\mu} - (\lambda + 2\mu) \sum_{\tau \in \mathcal{E}_H} \frac{\sigma_{\tau}}{H_{\tau}} \sum_{i=1}^2 \int_{\tau} (\mathbf{u}_i - \boldsymbol{\lambda}) \cdot \boldsymbol{\mu} = 0, \quad \forall \boldsymbol{\mu} \in H^{\frac{1}{2}}(\Gamma_{12})$$

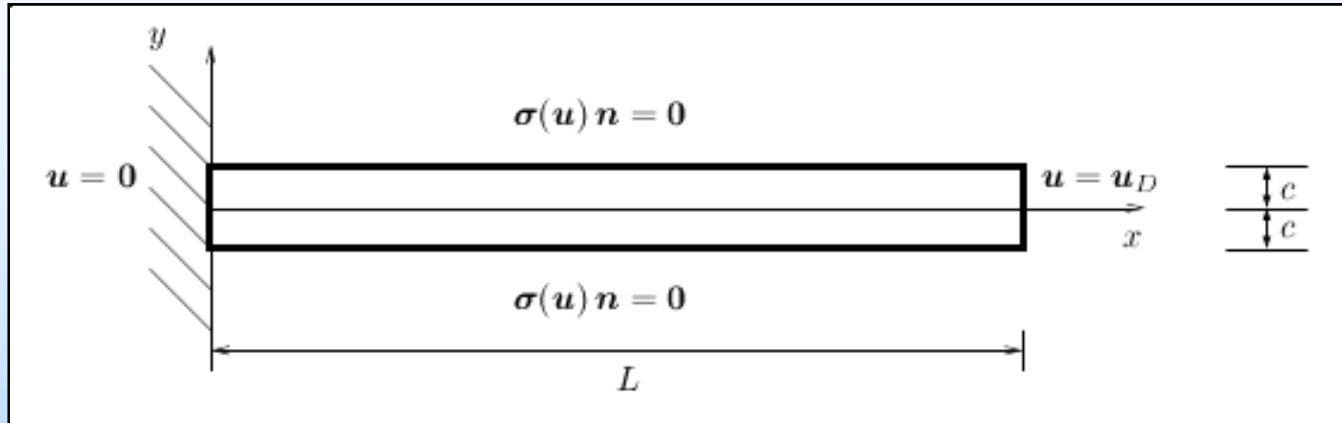
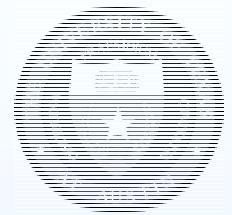
$$\begin{aligned}
 & |\mathbf{u}_h - \mathbf{u}|_{X_h} + \left((\lambda + 2\mu) \sum_{i=1}^2 \left(\sum_{\gamma \in \Gamma_{h,i}} \frac{\sigma_\gamma}{h_\gamma} \|\mathbf{u}_{h,i} - \mathbf{u}_D\|_{L^2(\gamma)}^2 \right. \right. \\
 & \left. \left. + \sum_{\gamma \in S_{h,i}} \frac{\sigma_\gamma}{h_\gamma} \|[\mathbf{u}_{h,i}]_\gamma\|_{L^2(\gamma)}^2 + \sum_{\tau \in \mathcal{E}_H} \frac{\sigma_\tau}{H_\tau} \|\mathbf{u}_{h,i} - \boldsymbol{\lambda}_H\|_{L^2(\tau)}^2 \right) \right)^{1/2} \\
 & \leq C \left(h^{r-1} \left(\left(\frac{h}{H} \right)^{1/2} + \left(\frac{H}{h} \right)^{1/2} \right) + H^{\bar{r}-1/2} Z \right),
 \end{aligned}$$

where $r = \min(k + 1, s)$ and $\bar{r} = \min(\ell + 1, s - 1/2)$

$Z = 1$, if DG strips are used

$Z = \left(\frac{H}{h} \right)^{1/2}$, if CG everywhere

Elastic Beam



$$\lambda = \frac{E\nu}{(1+\nu)(1-2\nu)}, \quad \mu = \frac{E}{2(1+\nu)}$$

$$E = 2.0\text{E}+5 \text{ N m}^{-2}$$

$$\mathbf{u} = \begin{pmatrix} -3\alpha x^2 y \\ \alpha x^3 + \frac{3\alpha\lambda}{\lambda+2\mu} x(y^2 - c^2) \end{pmatrix}$$

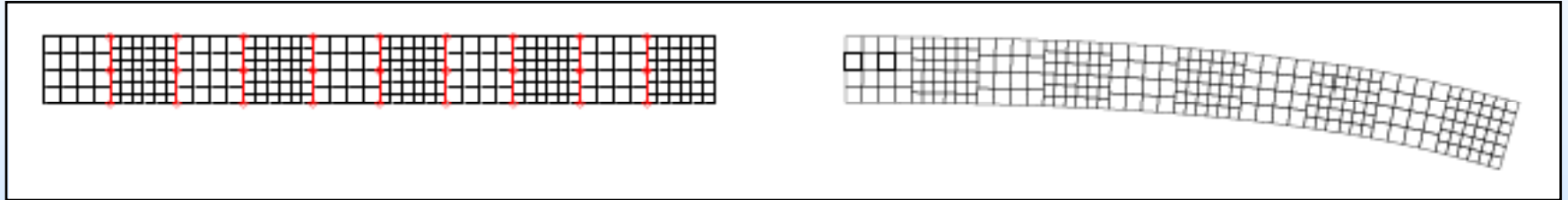
$$\nu = 0.3$$

$$L = 10 \text{ m}$$

$$\mathbf{f} = \begin{pmatrix} 6\alpha\mu \frac{3\lambda+4\mu}{\lambda+2\mu} y \\ 0 \end{pmatrix}$$

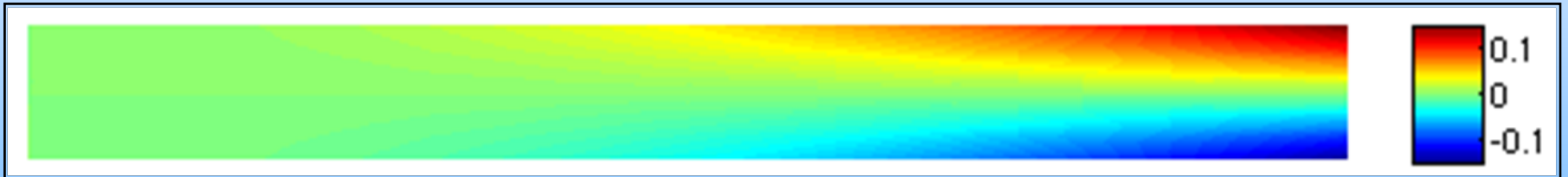
$$c = 0.5\text{m}$$

$$\alpha = -1.0\text{E}-3 \text{ m}^{-2}$$

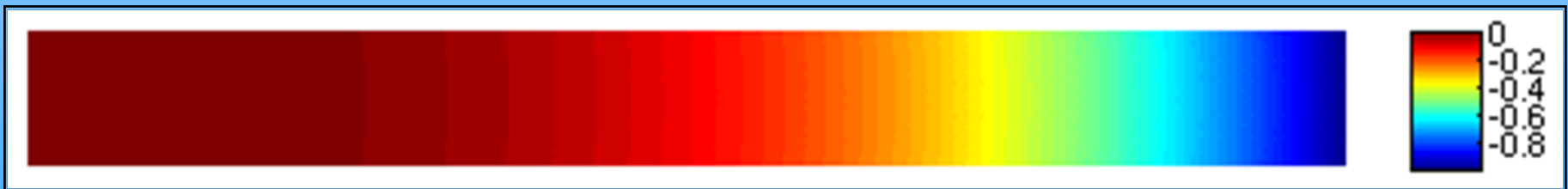


Initial subdomain & mortar mesh

Deformed mesh



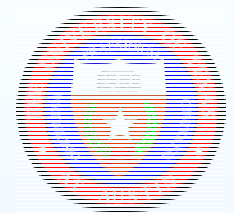
Displacement in x-direction



Displacement in y-direction



Convergence Rates



1/h	Rectangular mesh				Triangular mesh			
	l = 1		l = 2		l = 1		l = 2	
	Iter.	Error	Iter.	Error	Iter.	Error	Iter.	Error
4	45	3.98E+0	65	4.46E+0	44	1.10E+1	65	1.16E+1
8	60	1.53E+0	69	2.04E+0	59	3.87E+0	67	4.81E+0
16	78	6.52E-1	83	8.11E-1	79	1.40E+0	81	1.79E+0
32	106	3.05E-1	96	3.55E-1	107	6.46E-1	93	7.99E-1
64	146	1.48E-1	106	1.65E-1	148	3.24E-1	103	4.11E-1
128	205	7.33E-2	121	7.88E-2	207	1.57E-1	119	1.88E-1
OR		$\mathcal{O}(h^{1.14})$		$\mathcal{O}(h^{1.18})$		$\mathcal{O}(h^{1.21})$		$\mathcal{O}(h^{1.19})$
ER		$\mathcal{O}(h^{1.0})$		$\mathcal{O}(h^{0.7})$		$\mathcal{O}(h^{1.0})$		$\mathcal{O}(h^{0.7})$

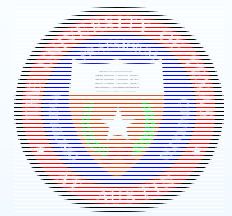
Linear
Subdomain
Approx.
(k=1)

1/h	Rectangular mesh				Triangular mesh			
	l = 1		l = 2		l = 1		l = 2	
	Iter.	Error	Iter.	Error	Iter.	Error	Iter.	Error
4	47	4.78E-1	73	1.44E-2	47	9.78E-1	72	1.05E-1
8	62	1.71E-1	101	3.10E-3	61	2.27E-1	96	1.14E-2
16	78	6.07E-2	136	6.83E-4	81	7.77E-2	132	2.40E-3
32	106	2.15E-2	189	1.60E-4	107	2.37E-2	185	5.35E-4
64	155	7.60E-3	264	3.85E-5	149	6.90E-3	260	1.26E-4
OR		$\mathcal{O}(h^{1.49})$		$\mathcal{O}(h^{2.14})$		$\mathcal{O}(h^{1.76})$		$\mathcal{O}(h^{2.38})$
ER		$\mathcal{O}(h^{1.5})$		$\mathcal{O}(h^{2.0})$		$\mathcal{O}(h^{1.5})$		$\mathcal{O}(h^{2.0})$

Quadratic
Subdomain
Approx.
(k=2)



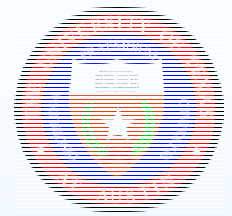
Conclusions



- ◆ Mortar methods defined and implemented for
 - Fully implicit multiscale method (MMFE) for multiphase flow coupled to a mixed/Godunov method for advection-diffusion-reaction problems on non-matching grids.
 - Elasticity
- ◆ Variably refined sub-domains results in significant savings in computational time (1 domain with fine grid takes twice the time as 3 domains) for multiphase flow coupled to reactive transport
 - Multiblock domain solution agrees very well with single-domain fine-everywhere
- ◆ Mortar approach allows for legacy code reuse and
 - Cheaper way to handle irregular geometries
 - Ideally suited for handling geological faults, fractures, etc.



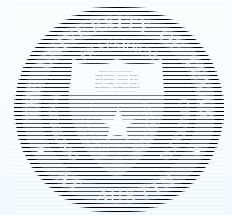
Current and Future Work



- ◆ Explore dynamic load balancing for treating reactions in parallel computations
- ◆ Apply error estimates for flow & transport to make suitable choice of sub-domain grids and mortar degrees of freedom
- ◆ Adding sharper *a posteriori* error estimators for adaptive mesh refinement (with M. Vohralík)
- ◆ Geomechanics model extensions to include permeability dependence on stress and coupling to nonisothermal EOS compositional flow model



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