



A level set method for fluid displacement in realistic porous media

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**Scaling up and modeling for transport and flow in
porous media**

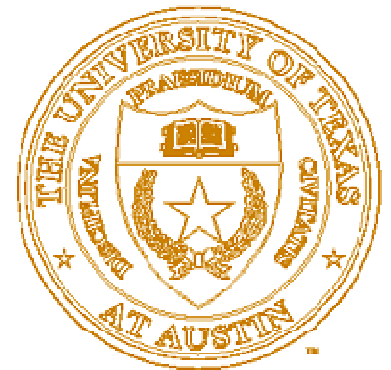
Dubrovnik, October 16, 2008

Joint work with

Steven Bryant, The University of Texas at Austin

Support

- US Department of Energy, grant "Mechanisms leading to coexistence of gas and hydrates in ocean sediments"
- US Department of Agriculture, grant "Quantifying the mechanisms of pathogen retention in unsaturated soils"



Computational resources

- Texas Advanced Computing Center (TACC)



Outline

- **Introduction**

- **Modeling**

- Level Set Method
- PQS Algorithm (Prodanović/Bryant '06)
- Contact angle modeling

- **Results**

- 2D
- 3D

- **Conclusions**

Pore scale immiscible fluid displacement

- Fluid-fluid interface (meniscus) at equilibrium with constant capillary pressure P_c and interfacial tension σ satisfies **Young-Laplace equation**

$$P_c = P_{nw} - P_w = \sigma \kappa$$

- Terminology: **wetting, non-wetting fluid, drainage, imbibition**
- We assume **quasi-static displacement**: at each stage interfaces are **constant mean curvature (κ) surfaces**

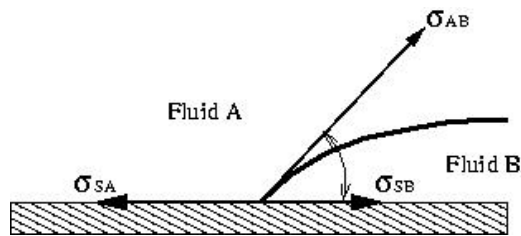


Fig.1. Contact angle at equilibrium

satisfies $\sigma_{AB} \cos \theta = \sigma_{SA} - \sigma_{SB}$



Statement of the problem

■ Goal

- **Accurately** model capillarity dominated fluid displacement in porous media

■ What is the big deal?

- Calculating constant curvature surfaces
- Modeling in irregular pore spaces
- Accounting for the splitting and merging of the interface within the pore space

■ What do we do?

- Adapt the **level set method** for quasi-static fluid displacement



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Level set method

- Osher & Sethian, '88: embed the moving interface as the zero level set of function Φ

- **The evolution PDE:**

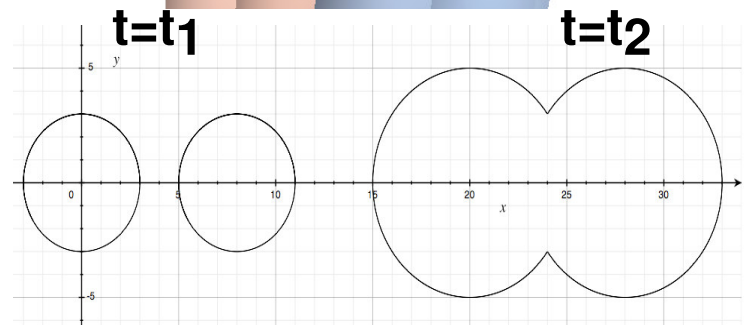
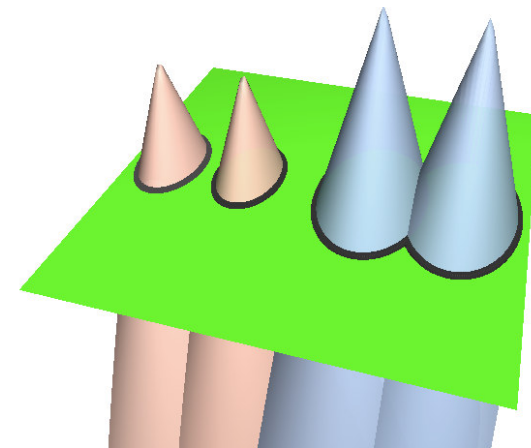
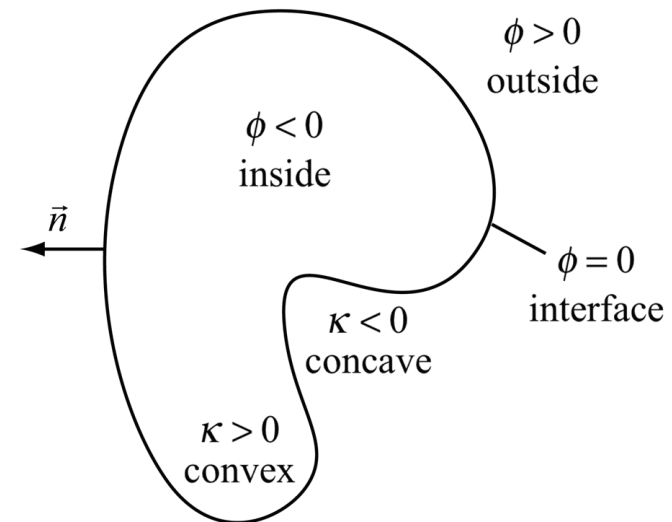
$$\phi_t + F|\nabla\phi| = 0, \quad \text{given } \phi(\vec{x}, 0)$$

- F is particle speed in the normal direction, e.g.

$$F(x, t) = p_c - \sigma\kappa(x, t)$$

- **Benefits:**

- works in any dimension
- no special treatment needed for topological changes
- (above F) finding const. curvature surface by solving a PDE



Progressive quasi-static algorithm (PQS)

■ Drainage

- Initialize with a planar front
- Solve evolution PDE with **slightly compressible curvature model for F** until steady state:

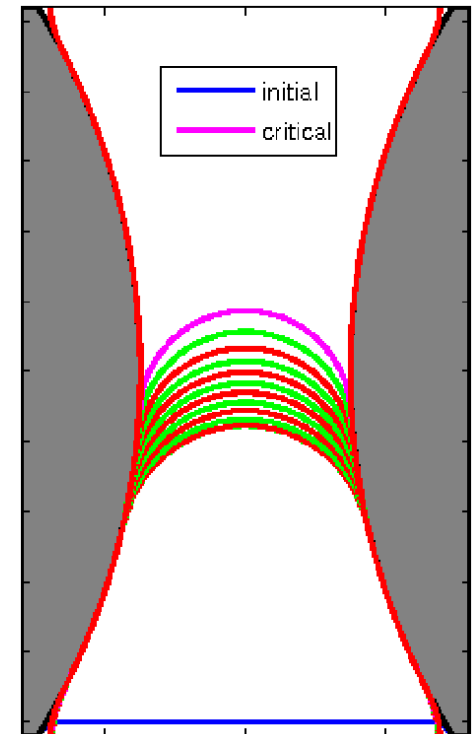
$$F(\vec{x}, t) = p_c \exp\left[f\left(1 - \frac{V(t)}{V_m}\right)\right] - \sigma \kappa(\vec{x}, t)$$

- Iterate

- increment curvature
- Find steady state of **prescribed curvature model**

$$F(x, t) = p_c - \sigma \kappa(x, t) = p_c - \sigma \nabla \cdot \frac{\nabla \phi}{|\nabla \phi|}$$

- **Imbibition** starts from drainage endpoint and decrements curvature
- Zero contact angle: **wall BC** $\phi = \max(\phi, \psi)$



M. Prodanović and S. L. Bryant. **A level set method for determining critical curvatures for drainage and imbibition.** *Journal of Colloid and Interface Science*, 304 (2006) 442--458.

Progressive quasi-static algorithm

non-zero contact angle

- Drainage

- Initialize with a planar front
- Solve evolution PDE with slightly compressible curvature model for F until steady state:

$$F(\vec{x}, t) = p_c \exp\left[f\left(1 - \frac{V(t)}{V_m}\right)\right] - \sigma \kappa(\vec{x}, t)$$

- Iterate

- increment curvature
- Find steady state of prescribed curvature model

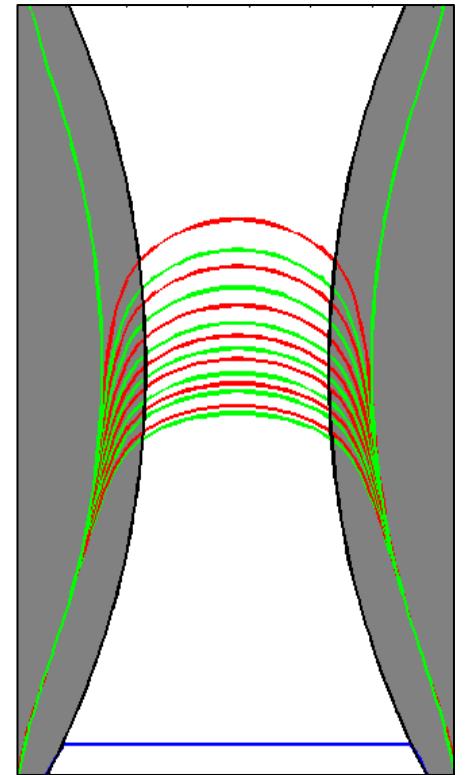
$$F(x, t) = p_c - \sigma \kappa(x, t) = p_c - \sigma \nabla \cdot \frac{\nabla \phi}{|\nabla \phi|}$$

- **Contact angle model**

$$F(\vec{x}, t) = p_c H(-\psi) - \nabla \cdot \left(\sigma(\psi) \frac{\nabla \phi}{|\nabla \phi|} \right)$$

$$\sigma(\psi) = \begin{cases} |\sigma_{SA} - \sigma_{SB}|, & \text{if } \psi \geq 0 \\ \sigma_{AB}, & \text{if } \psi < 0. \end{cases}$$

$$\sigma_{AB} \cos \theta = |\sigma_{SA} - \sigma_{SB}|$$





Software available

- LSMLIB Level Set Method Library

- K. T. Chu / M. Prodanović
- free for research, next release Jan 2009
- C/C++/Fortran (serial & parallel), Unix-like env.
- <http://www.princeton.edu/~ktchu/software/lsmllib/index.html>

- LSMPQS (Progressive Quasi-static alg.)

- first release planned Feb 2009



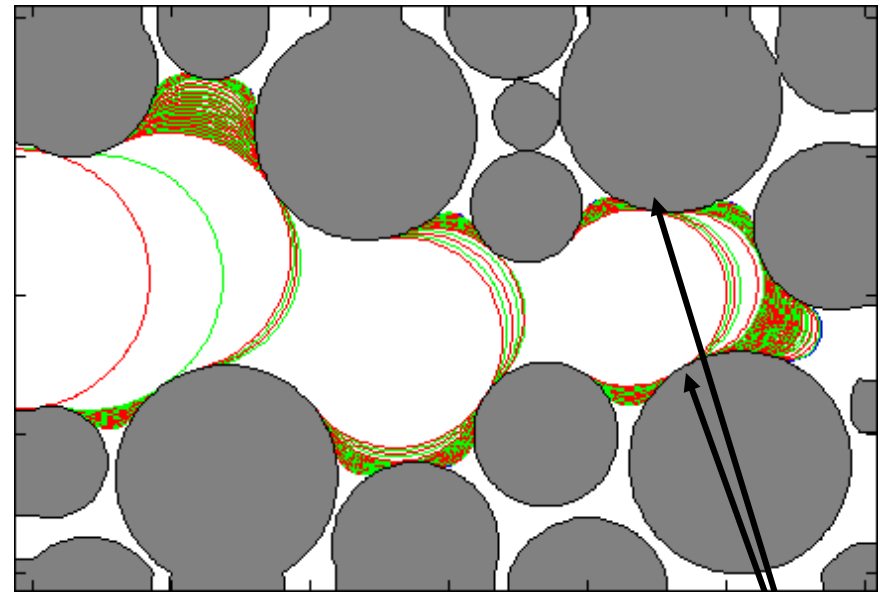
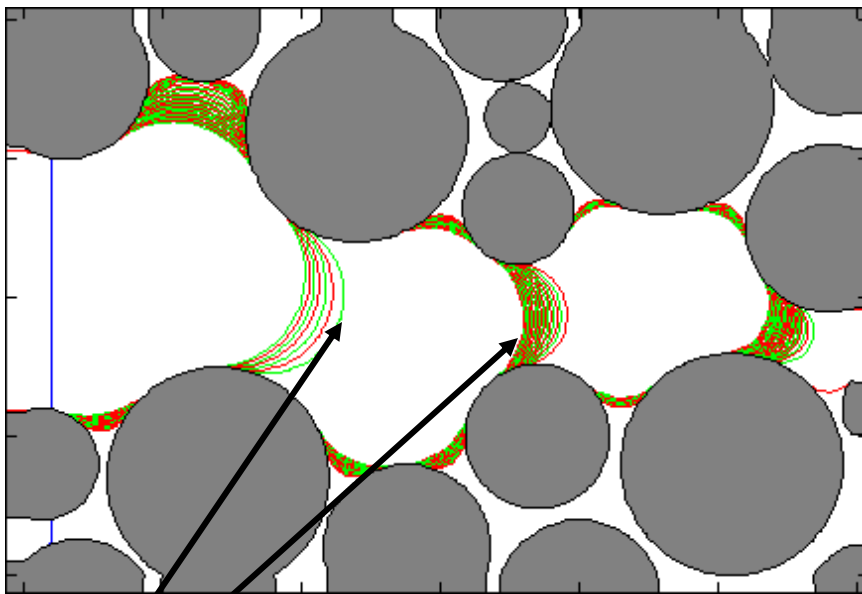
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2D Fracture ($\theta=0$)

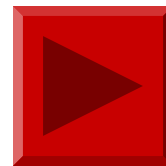
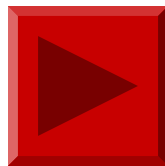
drainage (controlled by throats)

imbibition (controlled by pores)



Simulation steps (alternating red and green colors). All $\leq 2\%$ rel.abs.err.

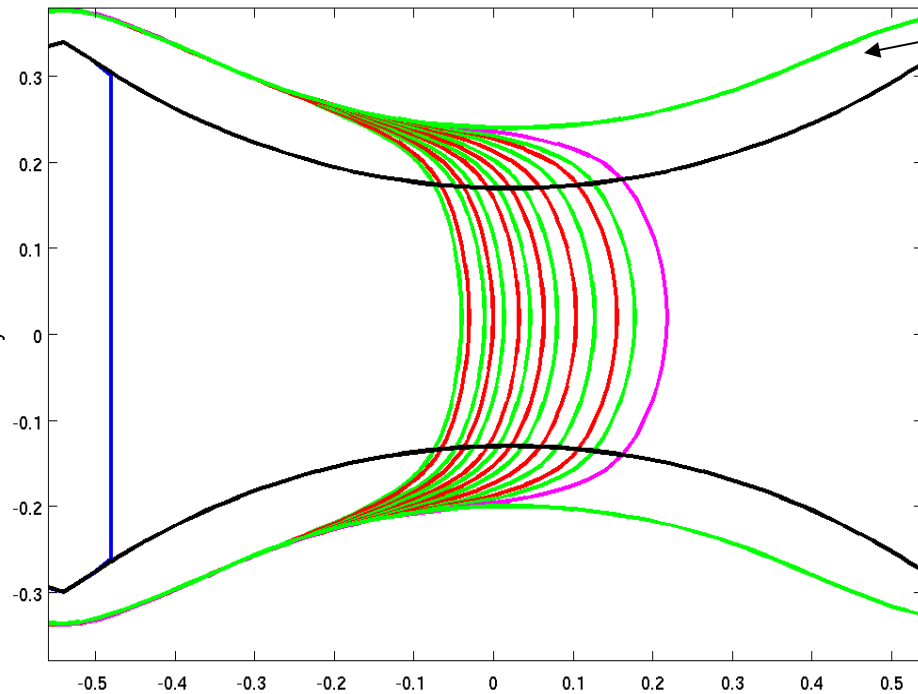
Haines jump



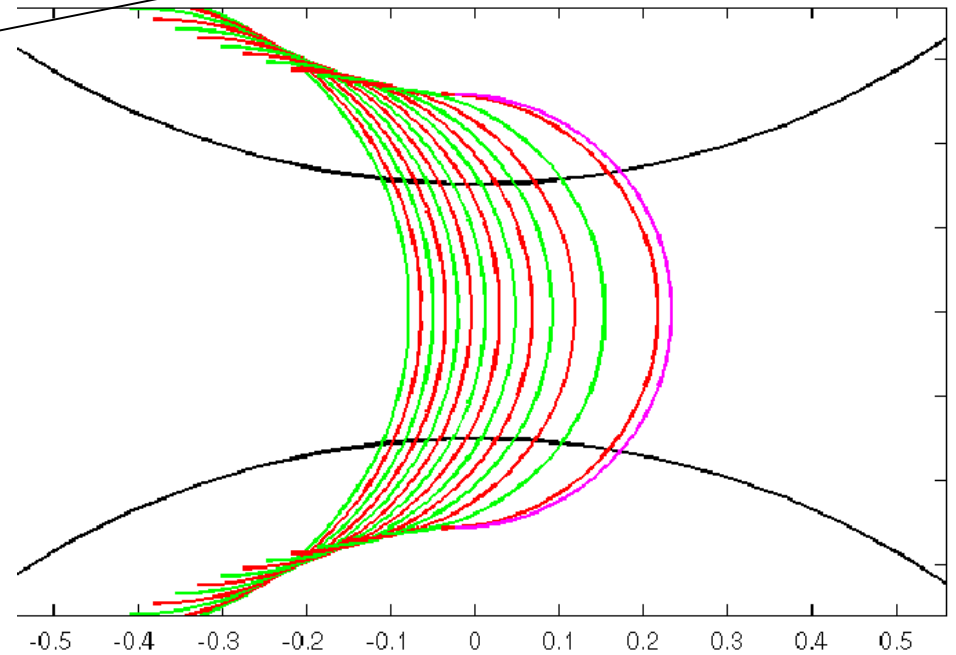
Melrose criterion

2D Throat: $\theta=60$

Some overlap
with solid allowed
in order to form
contact angle



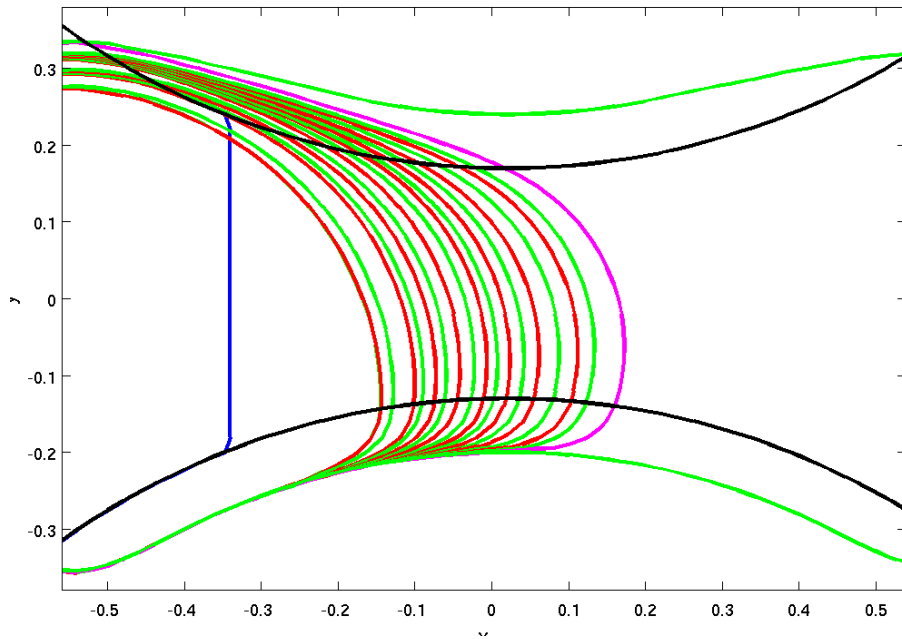
simulation, $C=3.88$



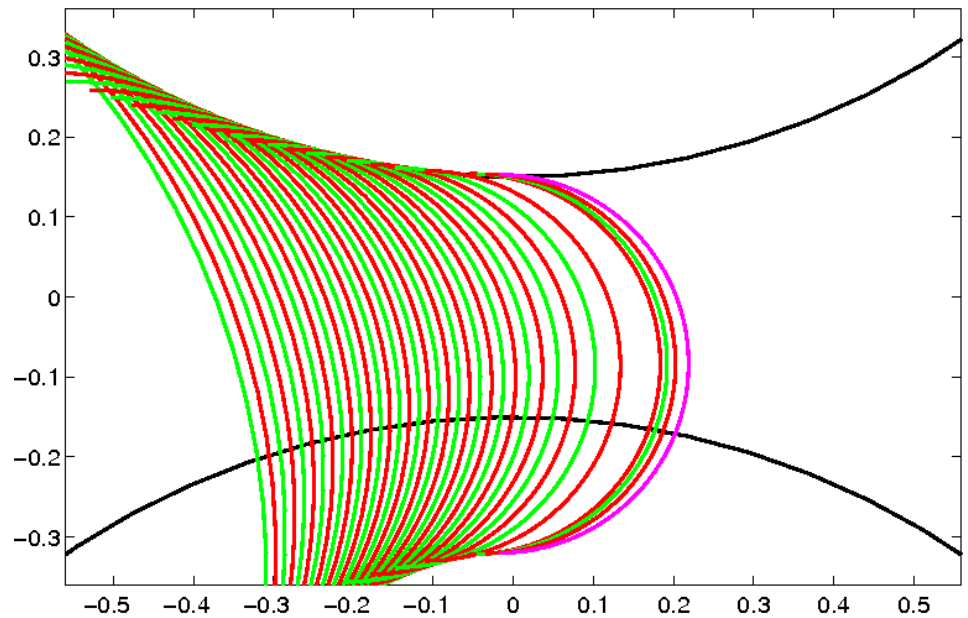
Analytic solution, $C=3.89$

The last stable meniscus shown in purple: not at geometrical throat!

Fractional wettability: $\theta=10$ and 80



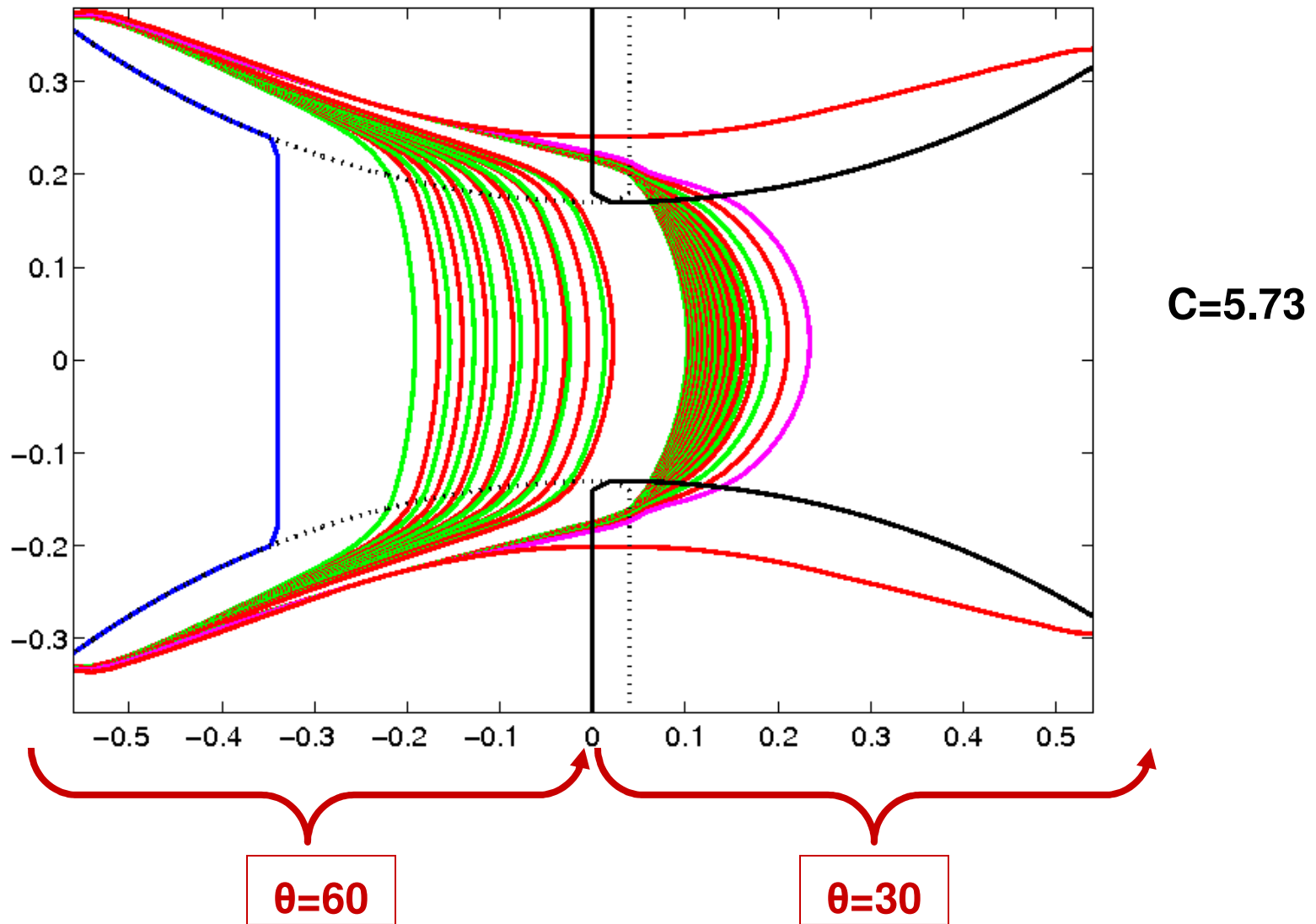
Simulation: $C=4.16$



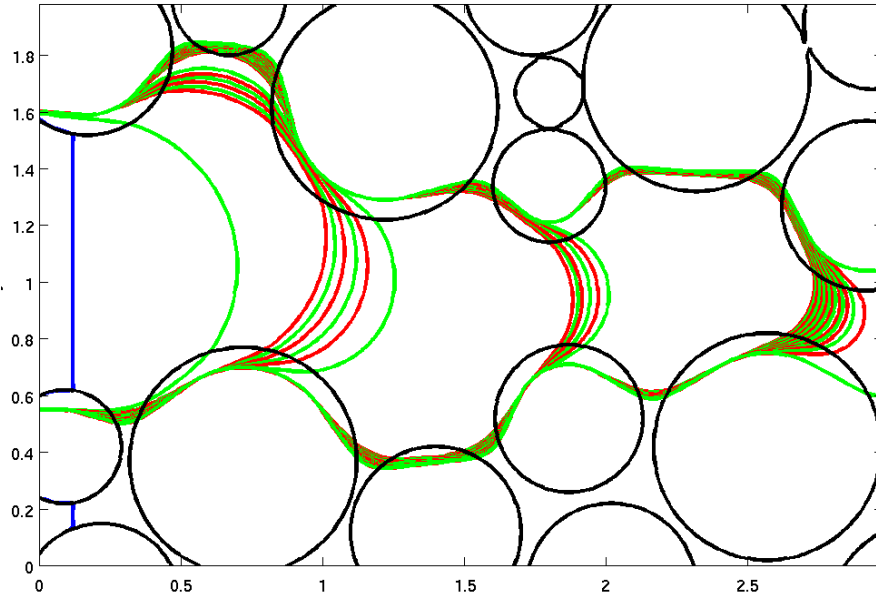
Analytic solution: 4.23

- Last stable meniscus shown in purple

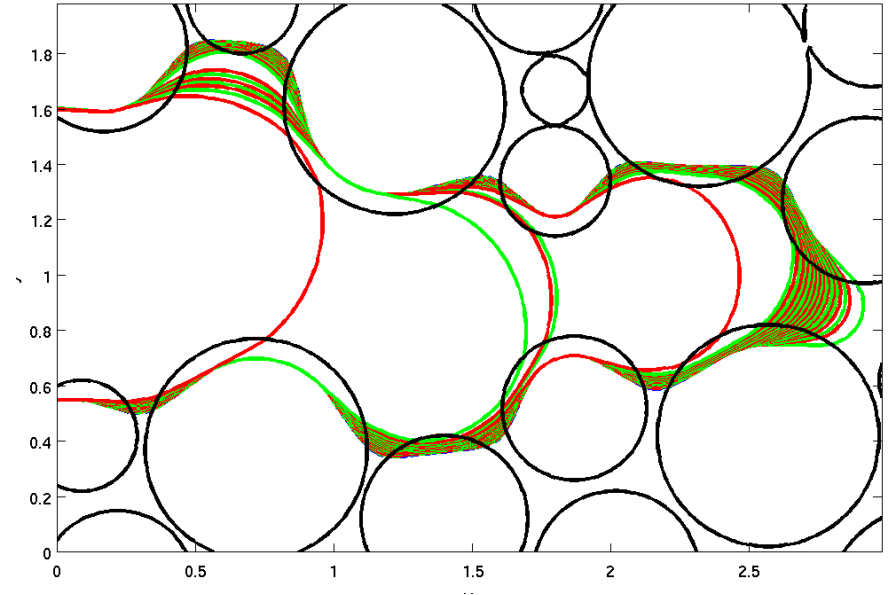
Mixed wettability: $\theta=60$ and 30



2D Fracture: $\theta=30$



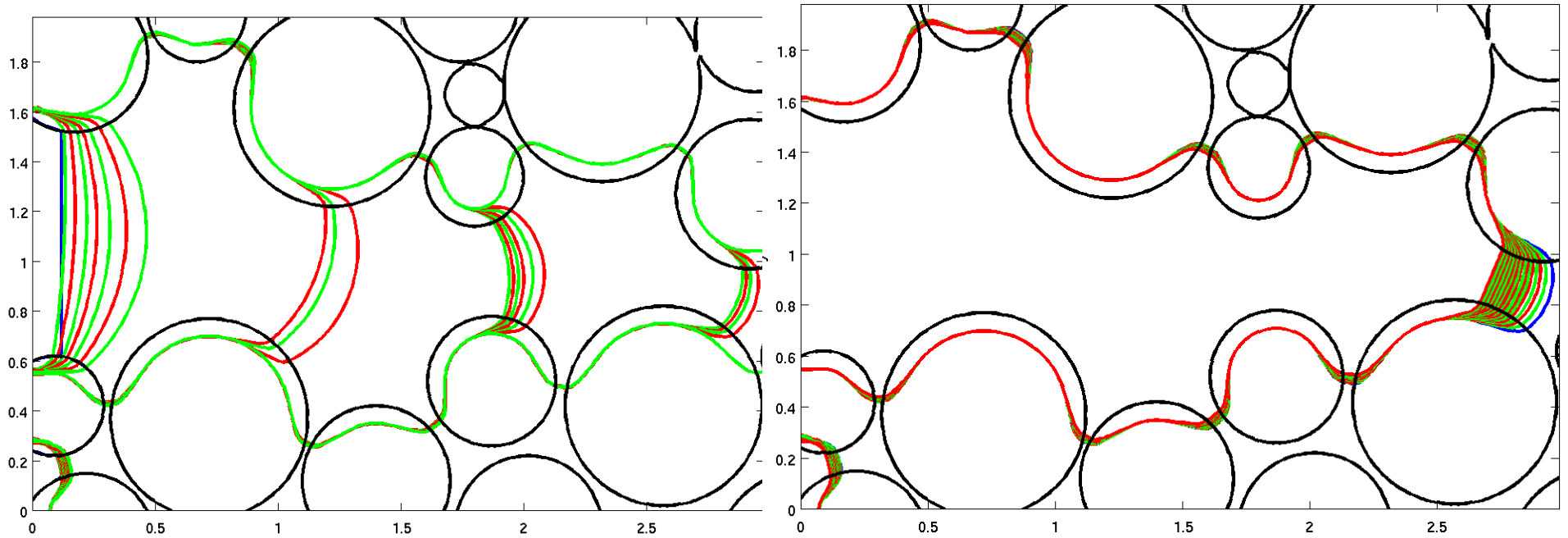
Drainage



Imbibition

- LSMPQS steps shown in alternate red and green colors

2D Fracture: $\theta=80$

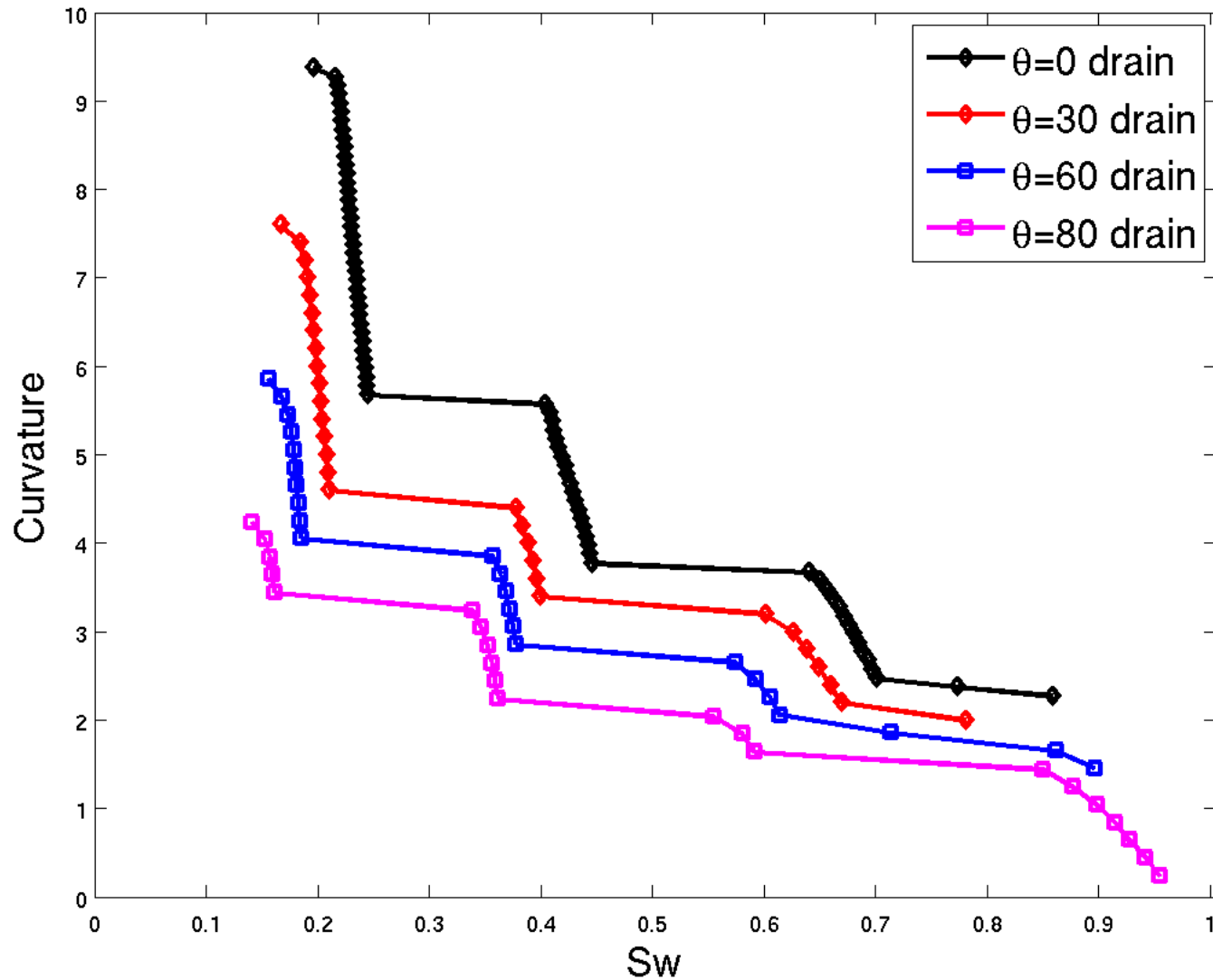


Drainage

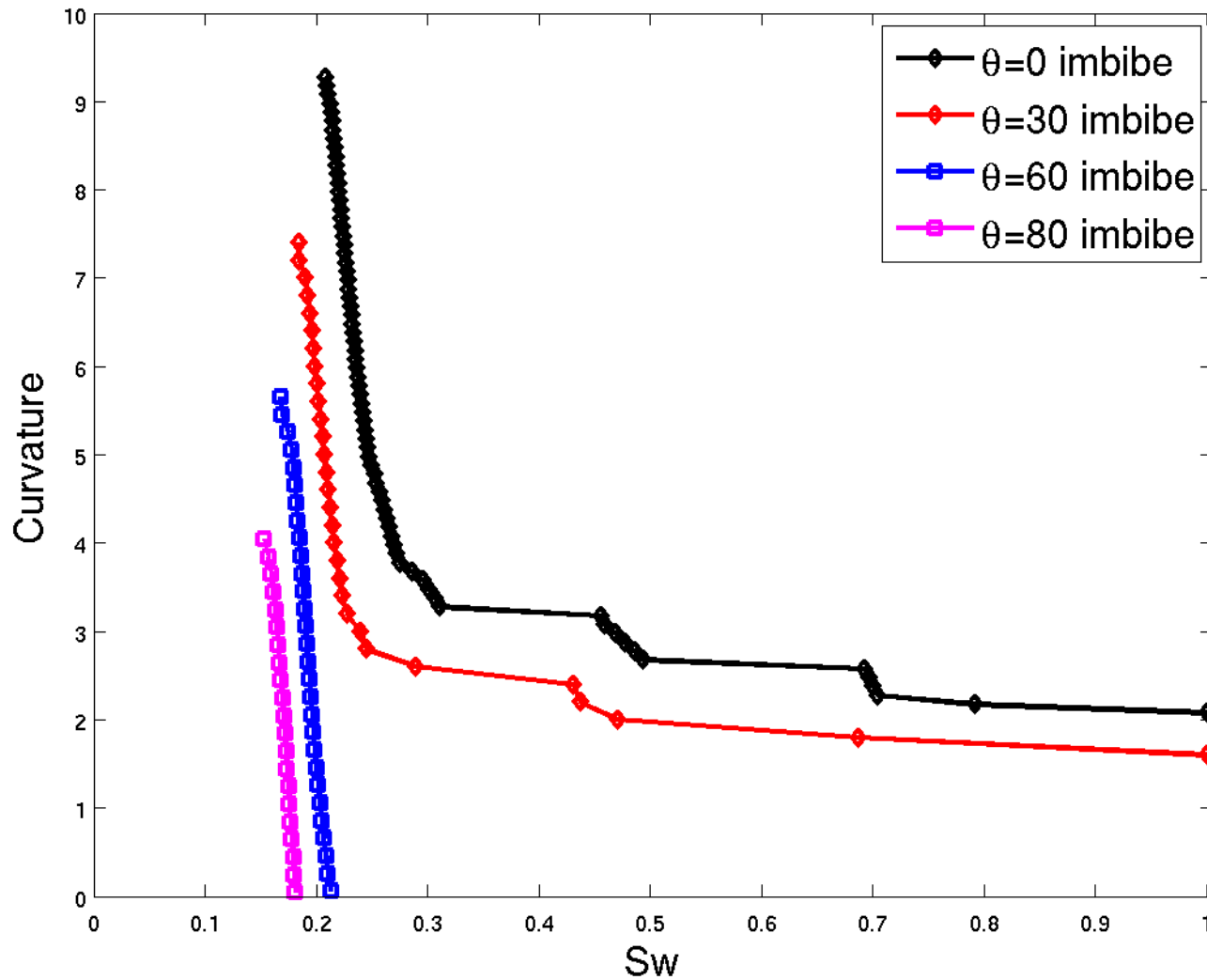
Imbibition: does not imbibe at a positive curvature!

- LSMPQS steps shown in alternate red and green colors

2D Fracture: drainage curves



2D Fracture: imbibition curves

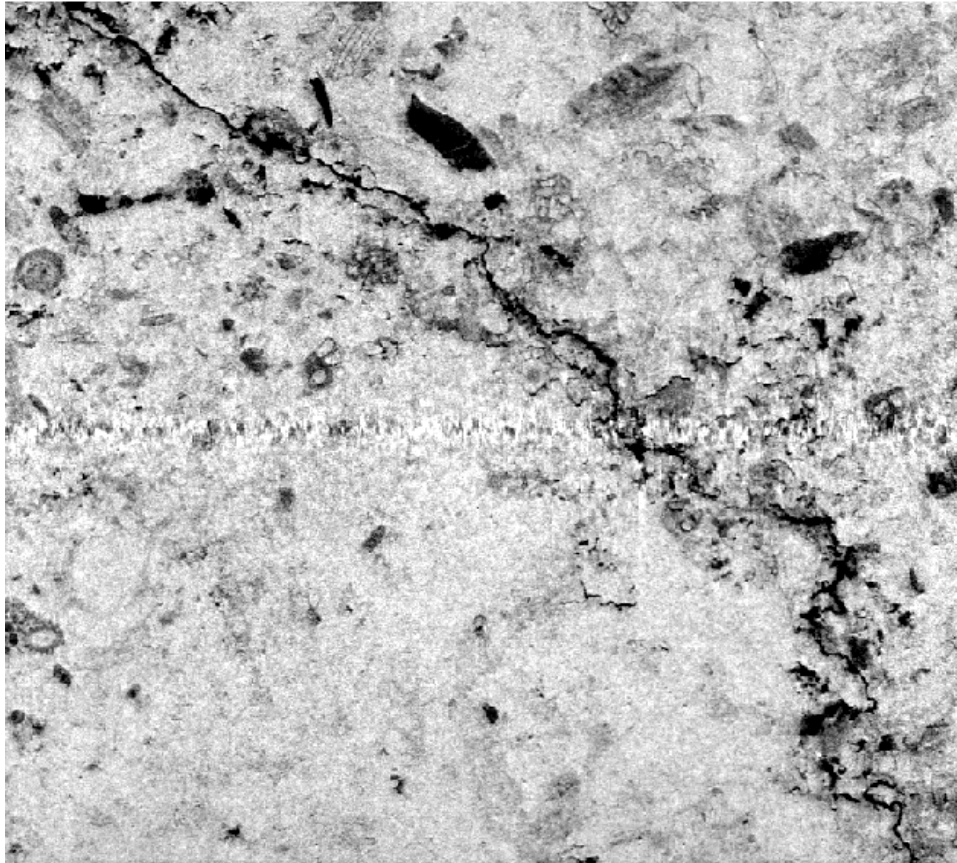




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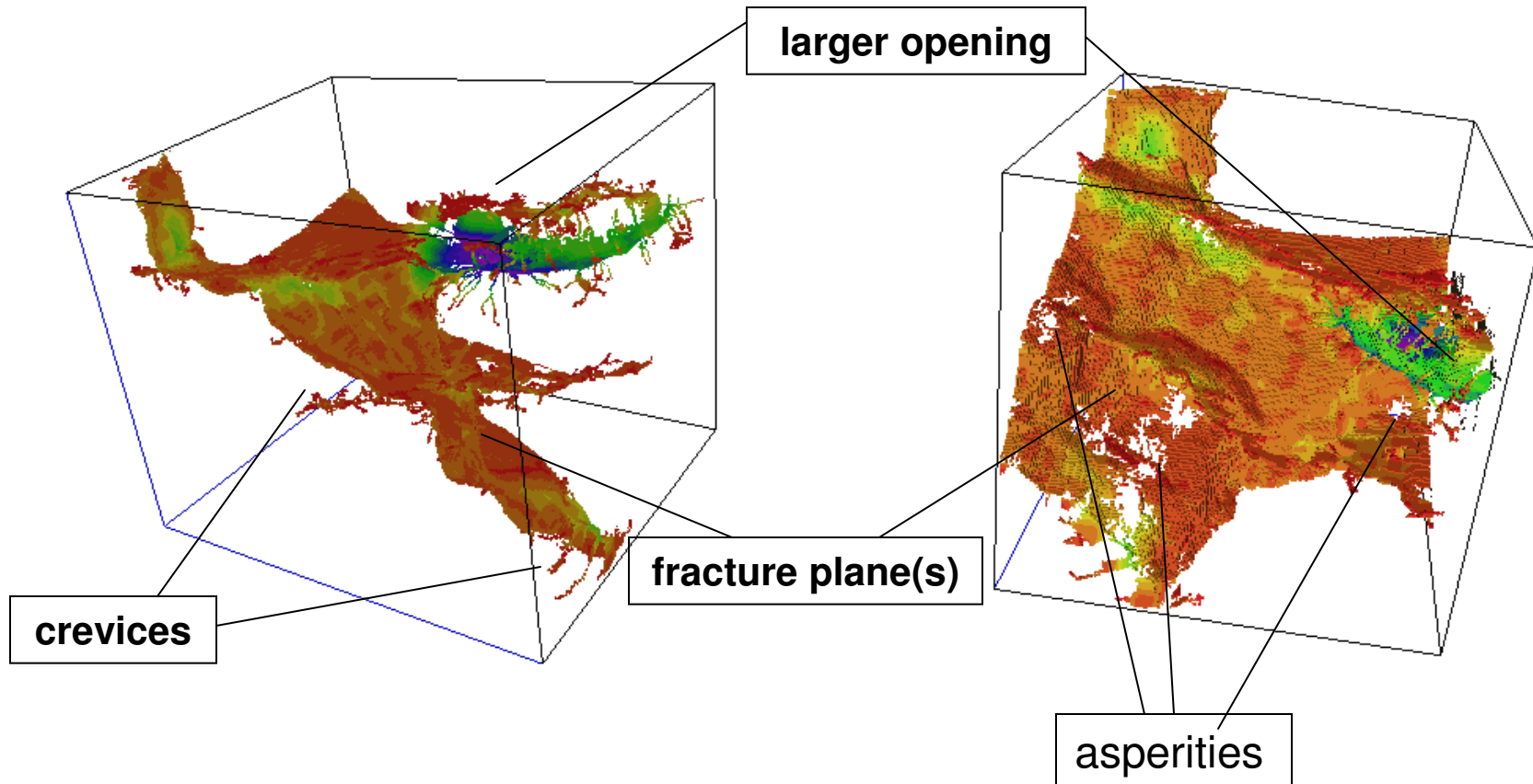
Naturally Fractured Carbonate



- original size 2048^3
- $dx = 3.1 \mu m$

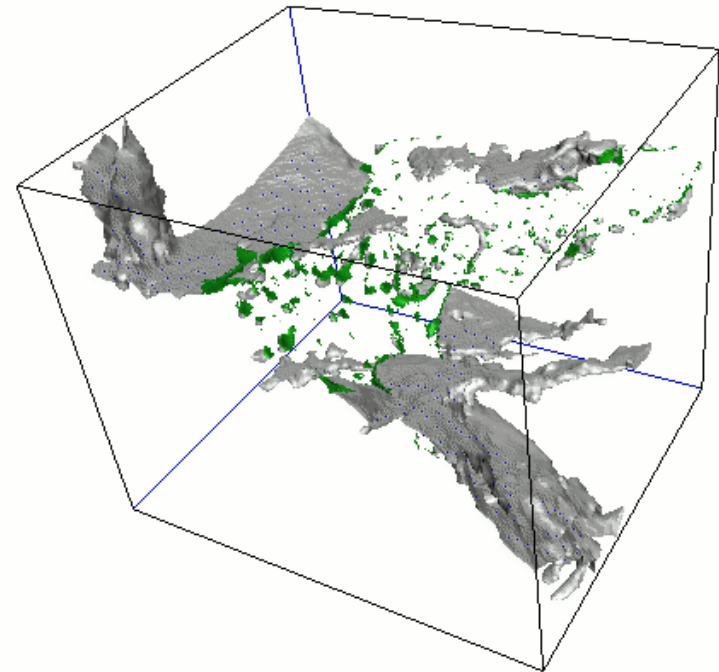
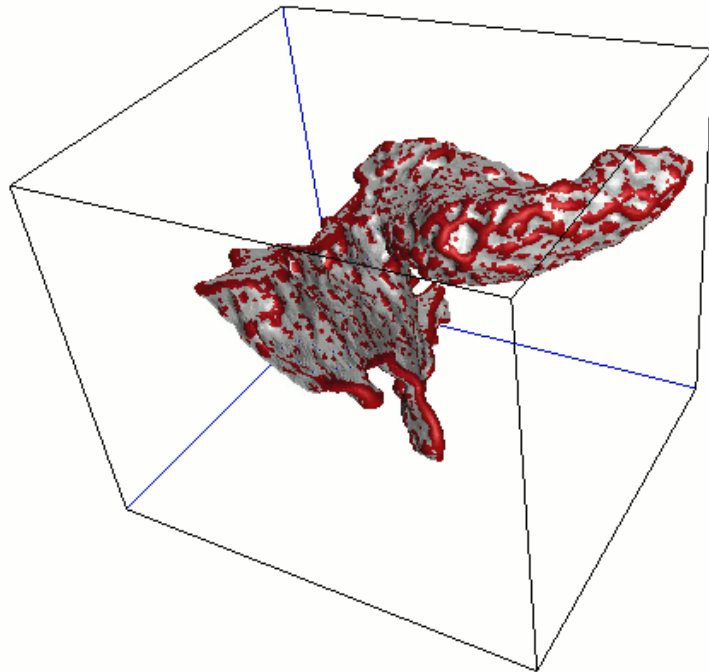
Image courtesy of Drs. M. Knackstedt & R. Sok, Australian National University

Fractured Carbonate Geometry

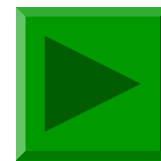
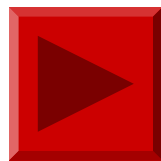


Medial surface of 200x230x190 subsample, rainbow coloring indicates distance to the grain (red close, violet far)

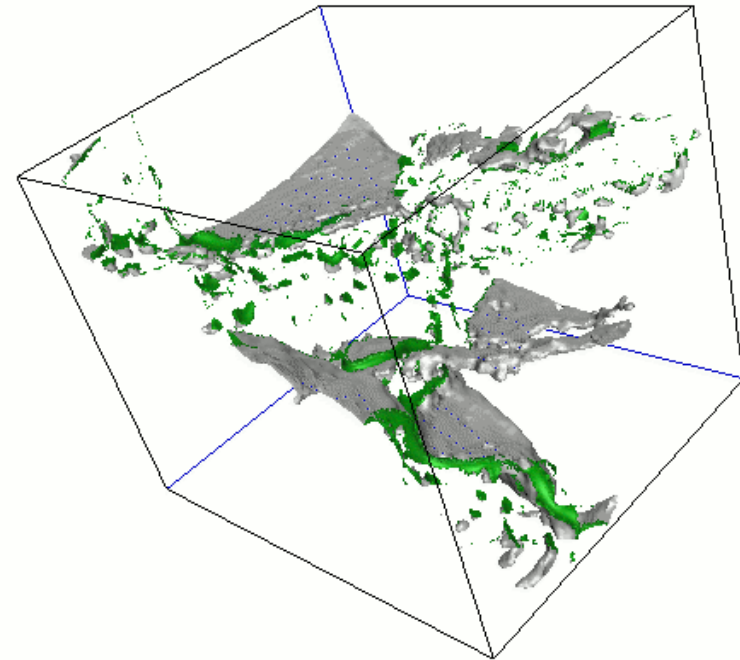
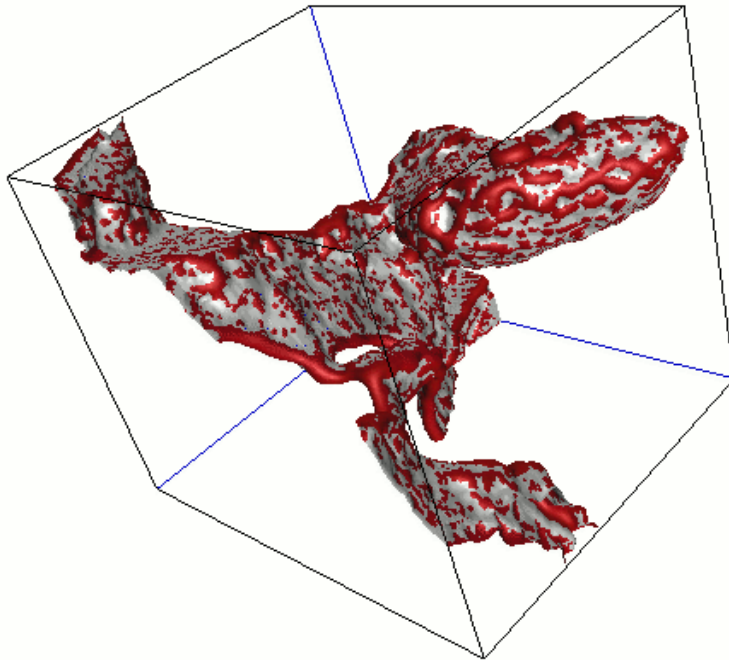
Fractured Carbonate Drainage



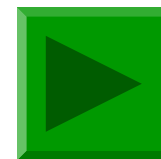
Non-wetting (left) and wetting phase surface (right) at $C_{16}=0.11\mu m^{-1}$



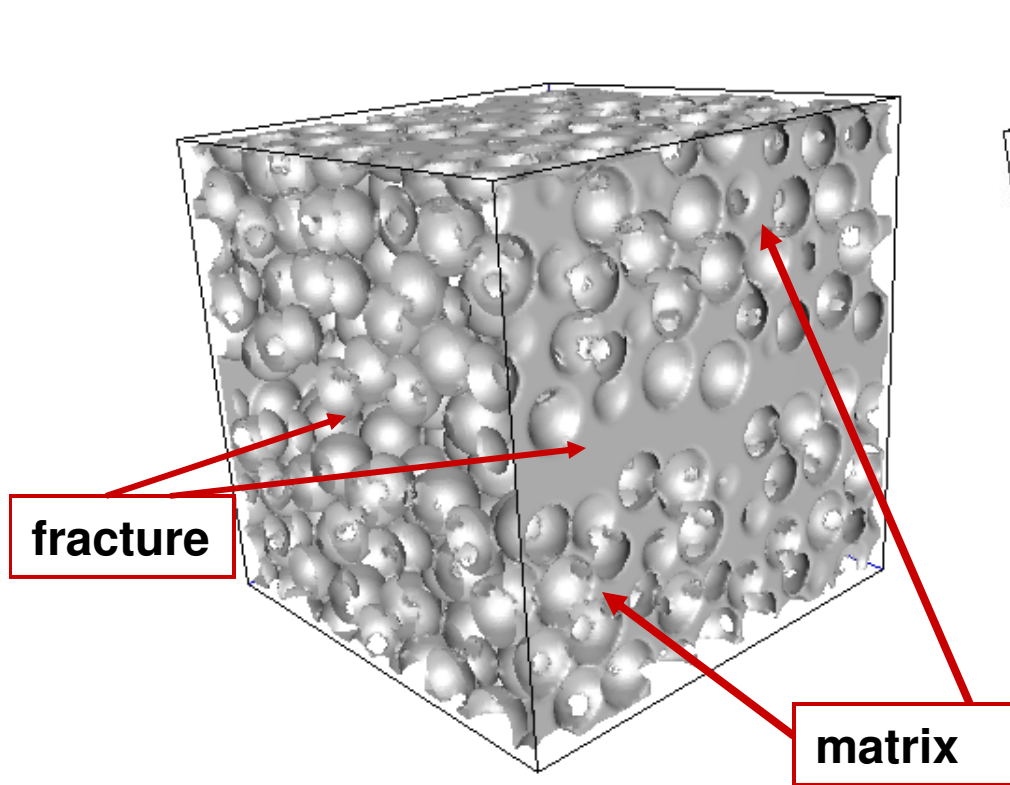
Fractured Carbonate Imbibition



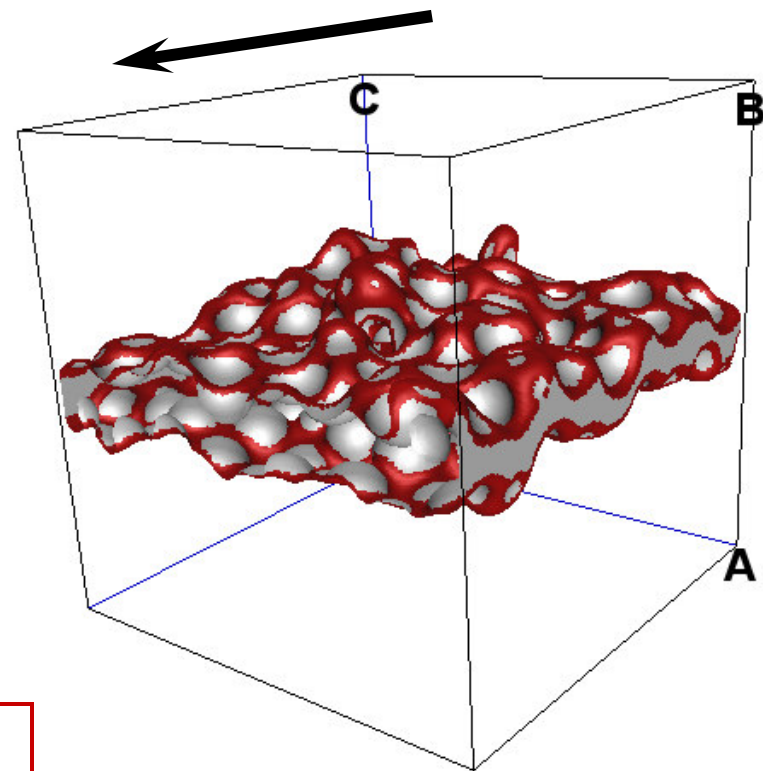
Non-wetting fluid (left) and wetting fluid (right) surface, $C_{15}=0.09\mu\text{m}^{-1}$



Fractured Sphere Pack

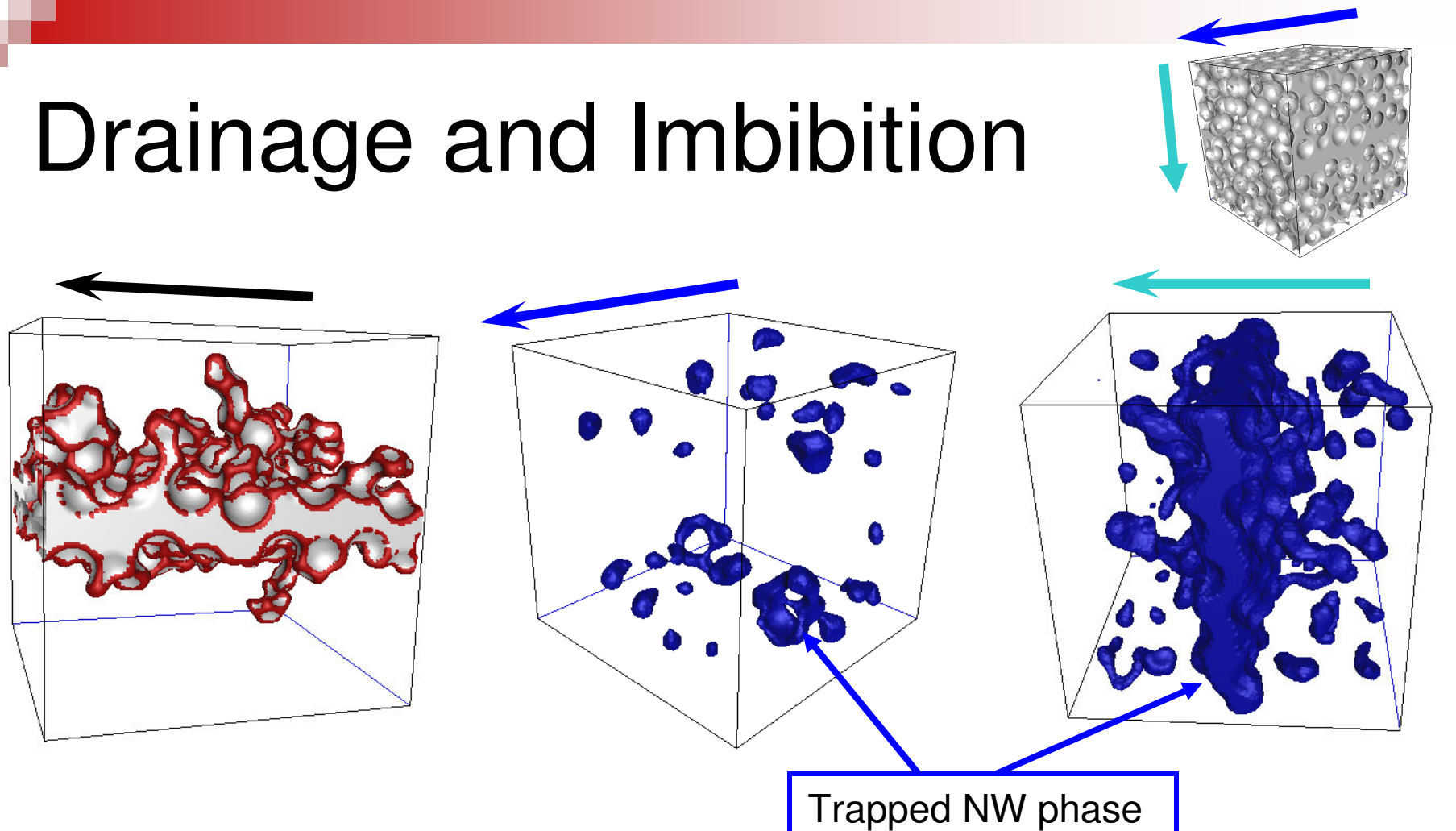


Pore-grain surface
sphere radii $R=1.0$
Image size 160^3 ($dx=0.1$)



NW phase surface in fracture
(drainage beginning)

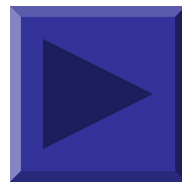
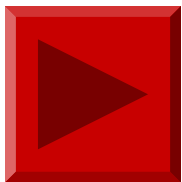
Drainage and Imbibition



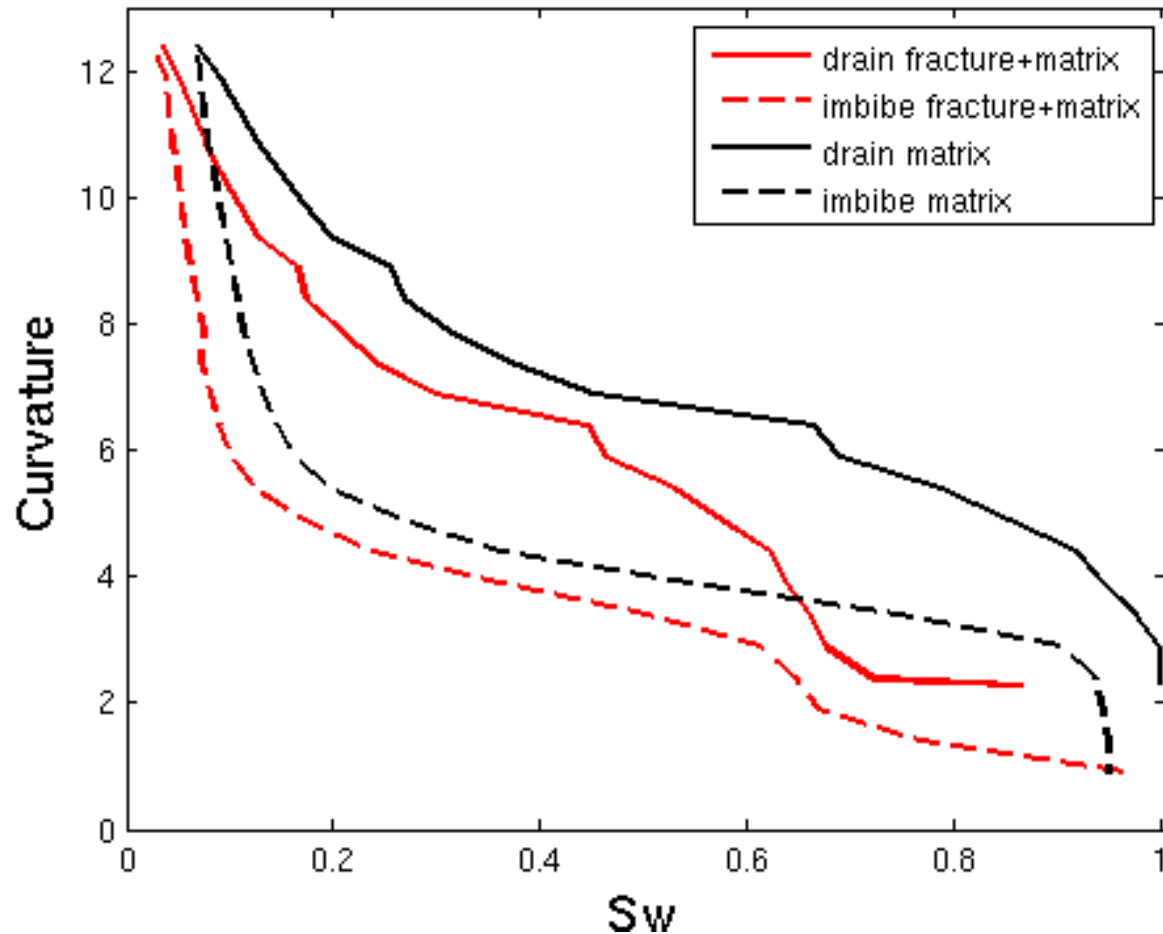
Drainage, $C=4.9$

imbibition, $C=0.24$

imbibition – rotated
 $C=2.15$

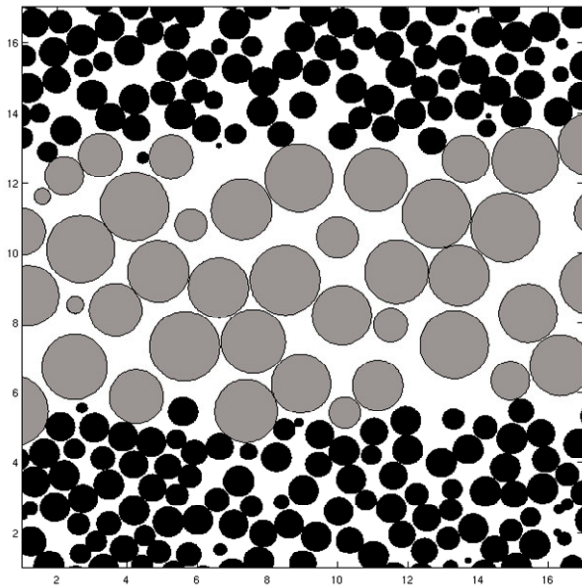


Simulated Pc-Sw: Fractured Sphere Pack



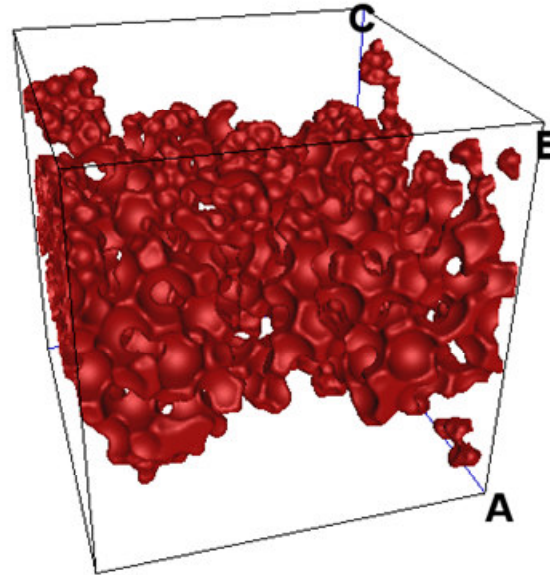
- In a reservoir simulation fracture+matrix curve might serve as an upscaled input (for a fractured system)

Fracture With Proppant: Drainage and Imbibition



(a)

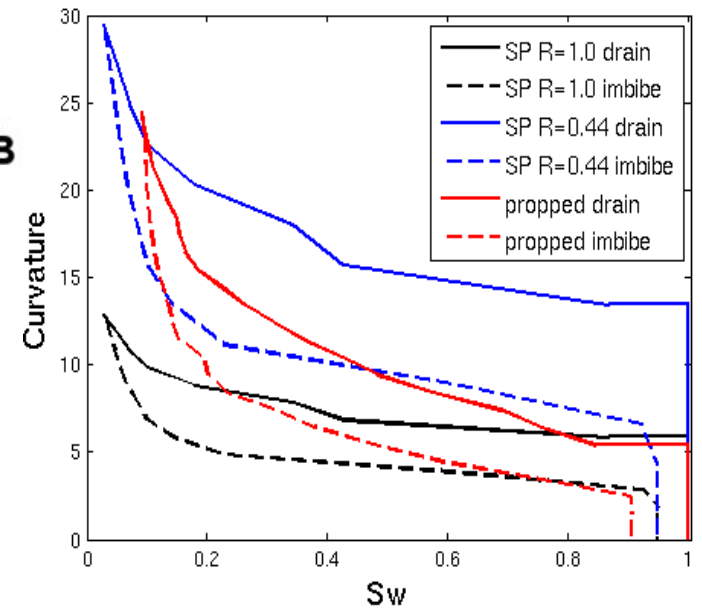
$$R_1 = 1.0$$
$$R_2 = 0.44$$



(b)

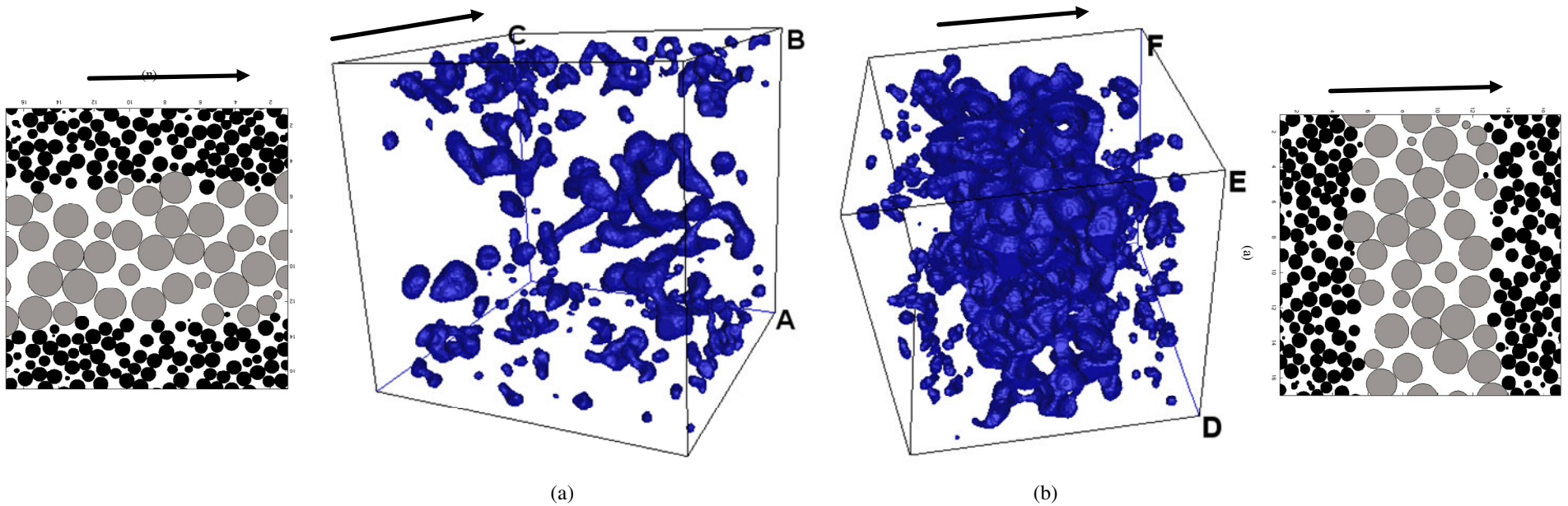
Drainage – matrix
began to drain

$$C=6.45$$



C- S_w curve for both
drainage and imbibition

Fracture With Proppant: Residual non-wetting phase



Residual oil at the imbibition endpoint for two directions of invasion



Conclusions

- **Drainage/imbibition modeling is**
 - Geometrically correct; Haines jumps, Melrose criterion
 - Robust with respect to geometry
- **We can easily obtain P_c - S_w curves, fluid configuration details (volumes, areas)**
- **Modeling (fractional & mixed) wettability possible**
- **Capillarity has an important effect on flow in rough wall fractures with contact points – we find W phase blobs around contacts and hysteresis of C- S_w curves**
- **The extent to which nonwetting phase is trapped in fracture/enclosed gaps is very sensitive to the direction of the displacement**
- **In a reservoir simulation the P_c - S_w curves in matrix+fracture system might serve as an upscaled drainage curve input for a fractured medium.**



Thank you!

More Info:

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